

# From MYRRHA to XT-ADS

Development of LBE cooled ADS and perspective of  
Implementation in Europe at Mol

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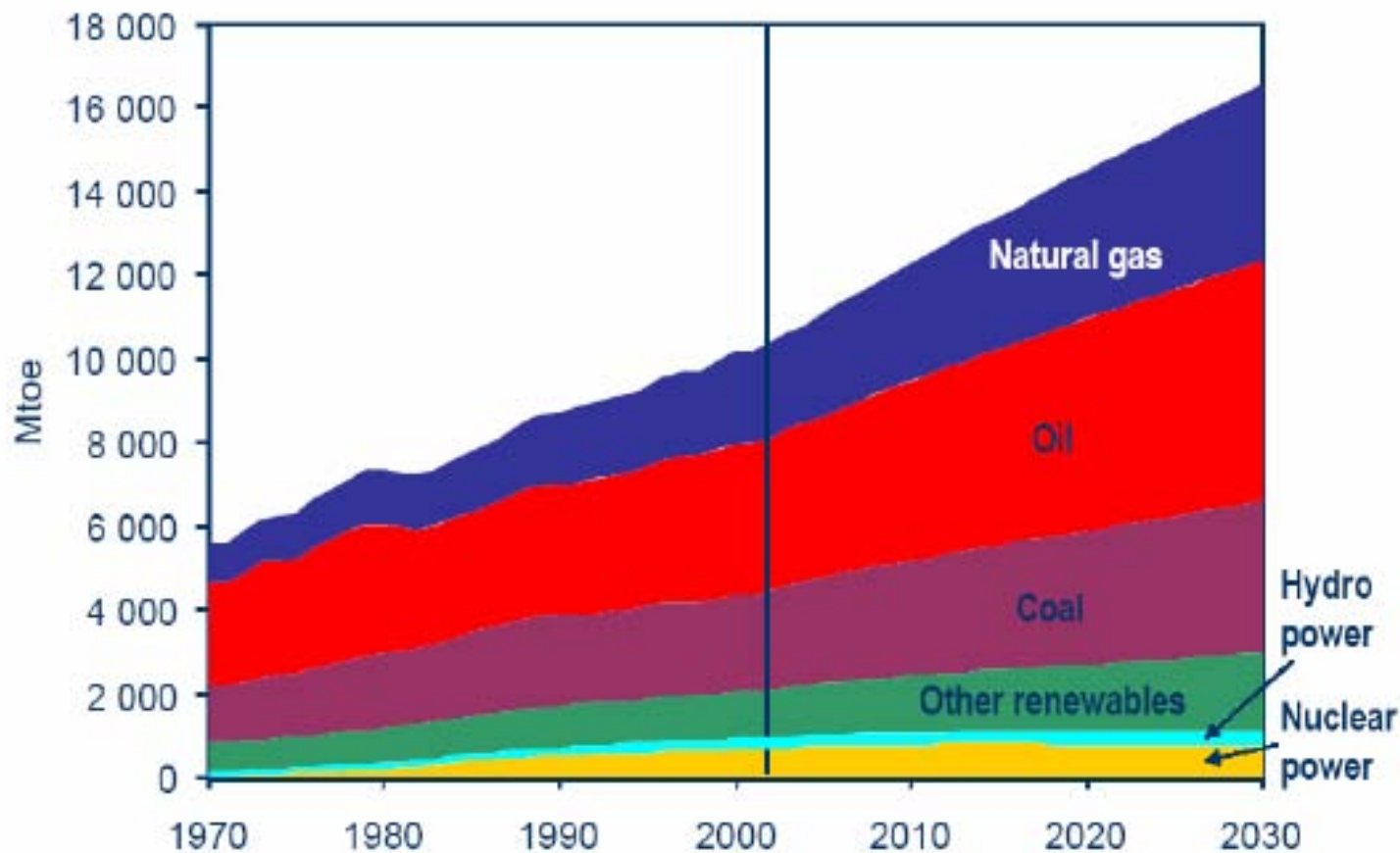
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- Introduction
- MYRRHA Components
- Perspectives for implementation
  1. SCK-CEN Commitment
  2. Opening to Europe
  3. Fast Spectrum Irradiation Facility
  4. Link ADS/Gen. IV LFR
  5. Comprehensive Support R&D
- Roadmap for deployment
- Conclusion

# World Primary Energy Demand until 2030, according to IEA



**Fossil fuels will continue to dominate the global energy mix,  
while oil remains the leading fuel**

# Cumulated CO<sub>2</sub> emissions from different means of electricity production



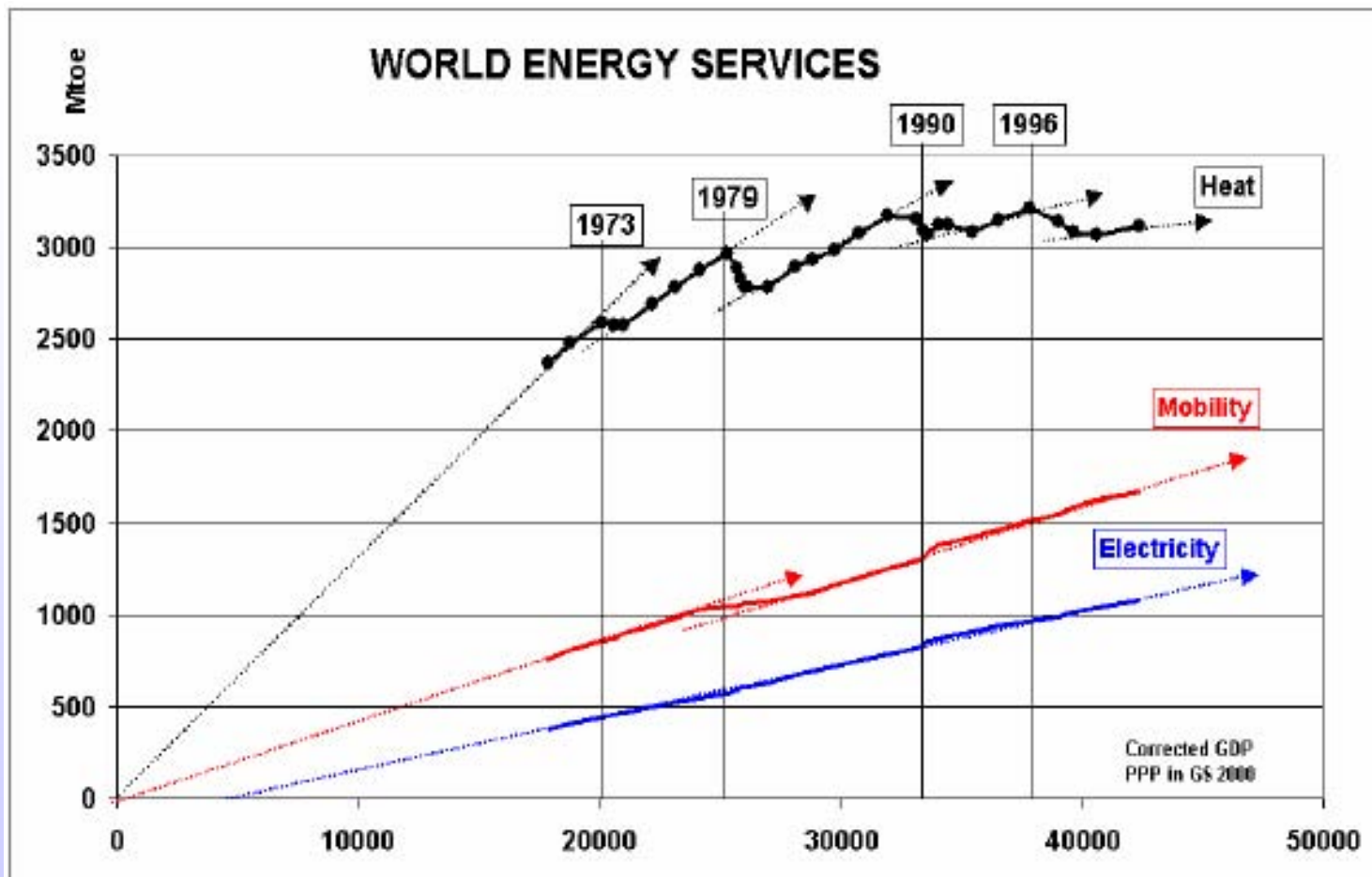
<u>Production Mode</u>	<u>grams CO<sub>2</sub> /kWh</u>
------------------------	----------------------------------

• Hydro-electricity	4
• Nuclear	6
• Wind	3-22
• Photovoltaic	60-150
• Combined-cycle gas turbine	427
• Natural gas direct-cycle	883
• Oil	891
• Coal	978

} Range reflects the assumption on how the large amount of energy for making the systems are generated!!

Source: SFEN, ACV-DRD Study

After the oil shock, global energy intensity has dropped down only in stationary uses of heat

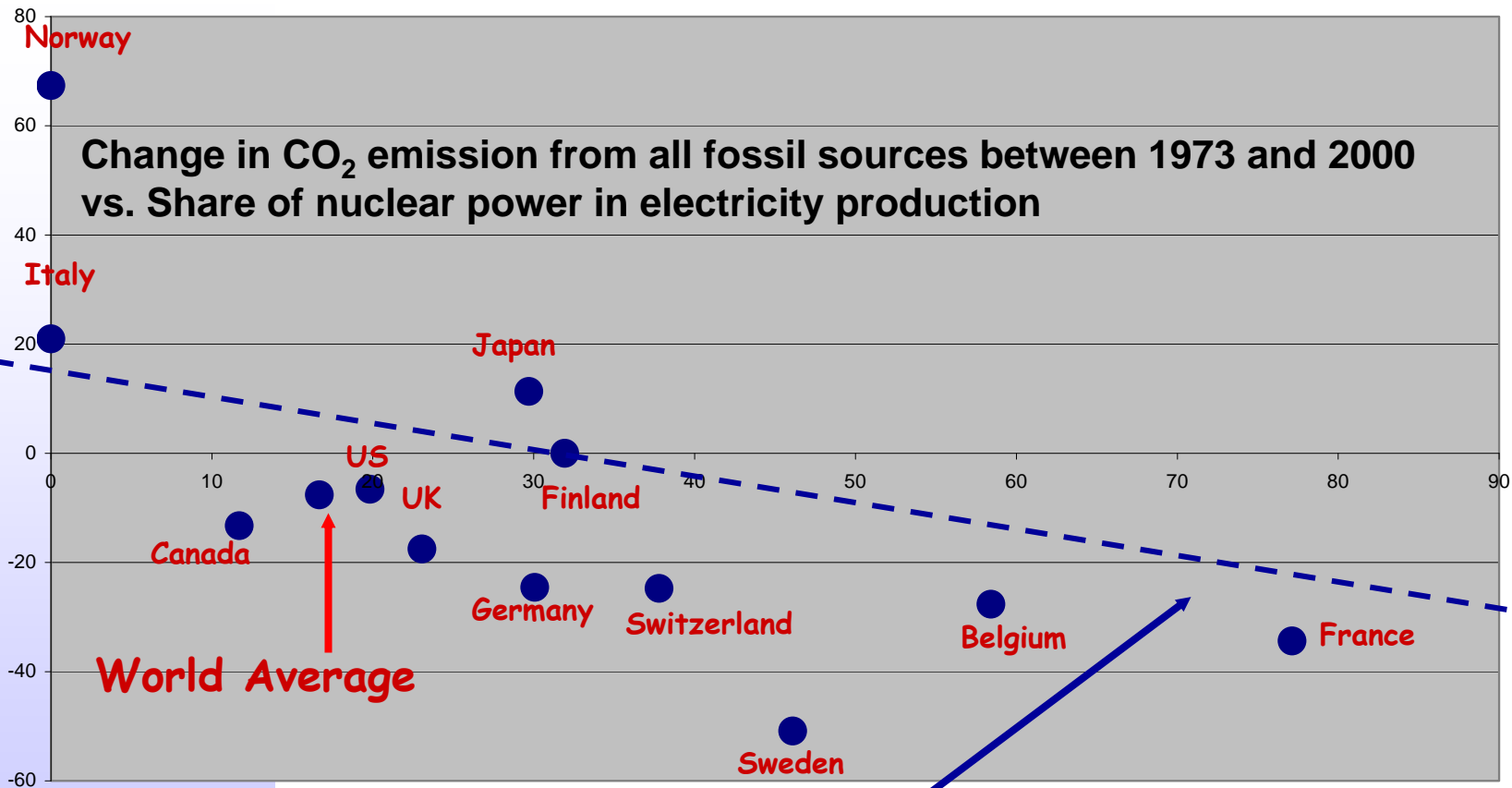


Source: WEC, Drivers of the Energy Scene, Dec. 2003

# Introduction of Nuclear Power and Reduction of CO<sub>2</sub>-emission



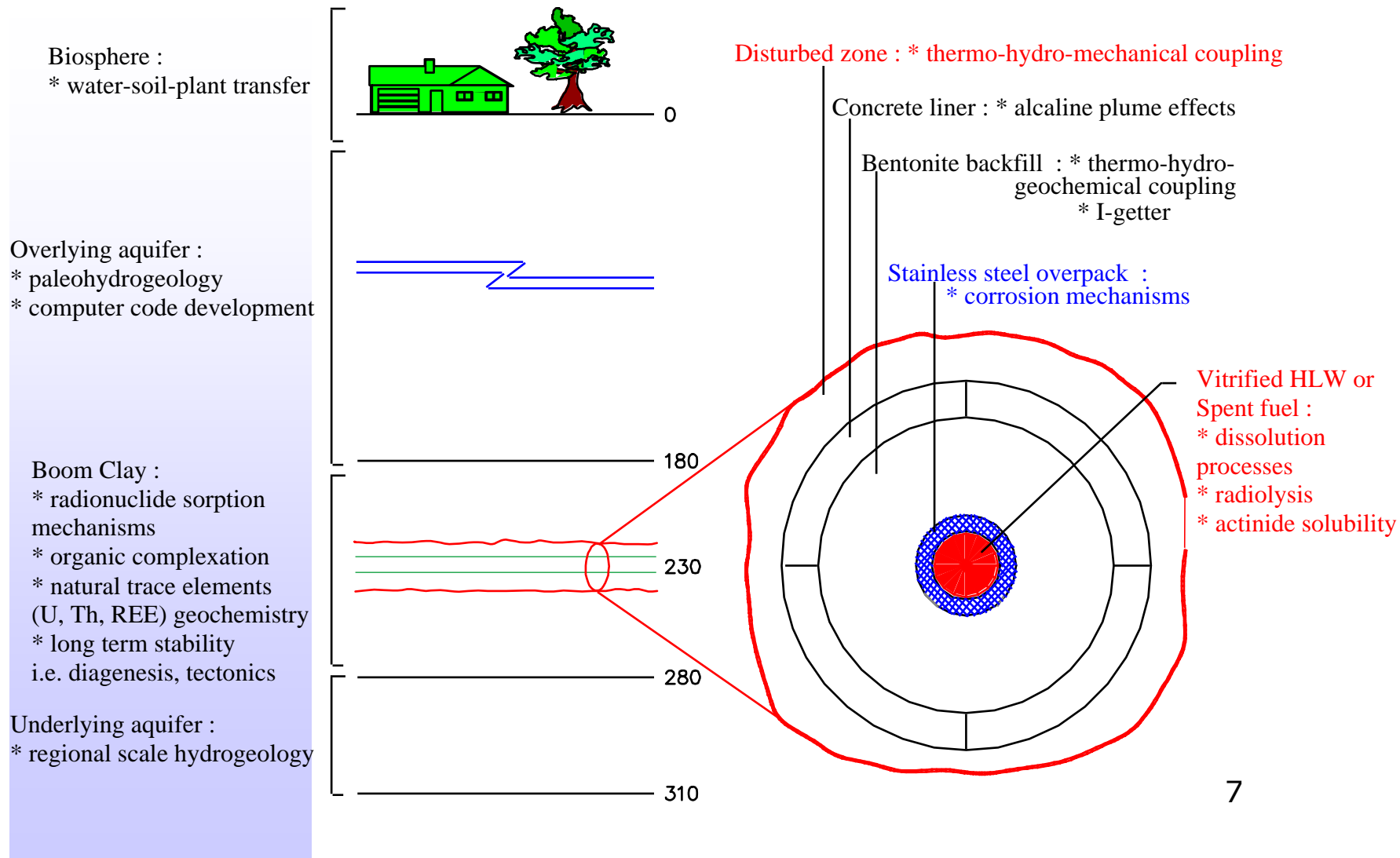
Data: Change from ORNL, Marland et al.  
Nuclear Share from EIA, DOE



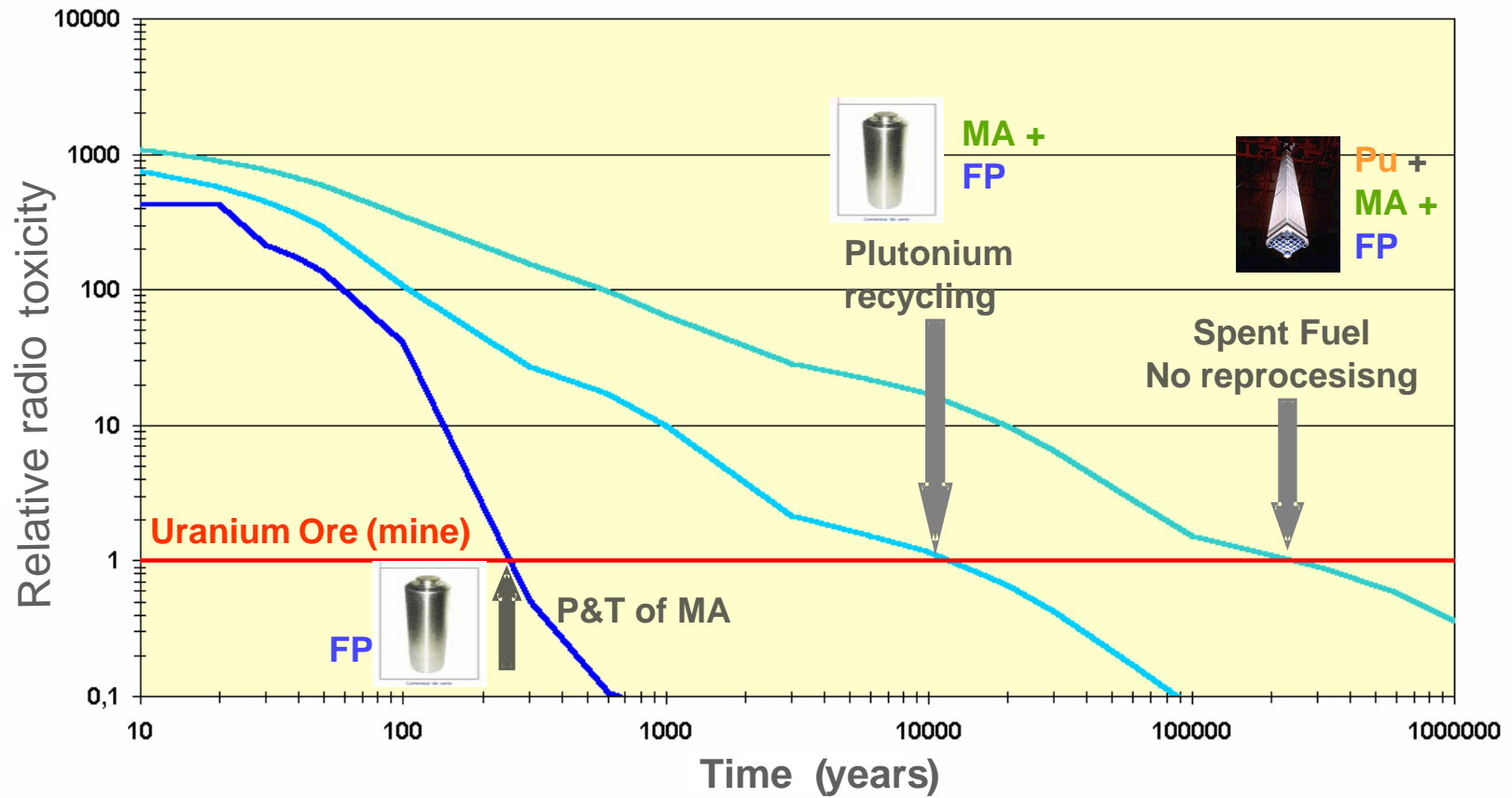
Is this trend only suggestive or a reality ?

# Is there a Solution for HLW?

YES



# The Problem is the Public acceptance





# Estimation Of Amount of Waste Form: Japanese Case study



## (1) “Reference” case

- Conventional reprocessing by PUREX process
- Recovery efficiency of U and Pu : 99.5 %.
- Conventional glass waste form was assumed as the HLW.

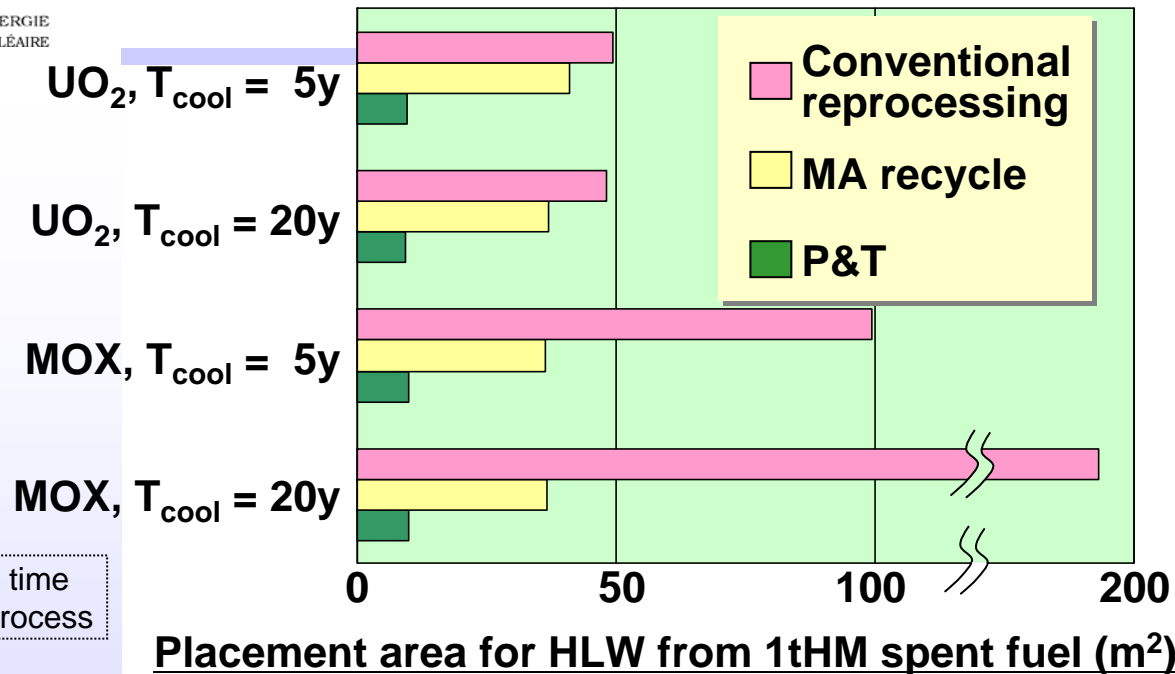
## (2) “MA recycle” case

- MA was recovered and recycled with Pu.
- Recovery efficiency of MA: 99%
- Recovery efficiency of U and Pu : 99.5 %.
- Glass waste form containing FP and small amount of MA was assumed as the HLW.

## (3) “MA+FP P&T” case

- HLW from “Reference case” were divided into 7 categories by partitioning.

# Estimation of Reduction of Total Repository Area



T<sub>cool</sub> : Cooling time before process

- The area for “MA+FP P&T” case is dominated by Cs and Sr.
- The total area for “MA+FP P&T” case is 1/5 - 1/26 of the “Reference” case and about 1/4 of the “MA recycle” case, even if Tc-PGM is disposed.
- The extension of the repository life-time or capacity is expected. For example, one deep underground repository of 2 km<sup>2</sup>, can be effective for 200 years in “MA+FP P&T”, assuming a reprocessing plant of 1,000tHM/y, while one site would be necessary in every 40 years in the conventional case.

# Estimation of Repository Area: Results of Total Area

## Placement area of deep underground repository for HLW from 1 tHM of spent fuel (Unit: m<sup>2</sup>)

Fuel	Cooling period	Reference	MA recycle	MA+FP P&T					
		HLW	HLW	(b) Tc-PGM	(c) Cs	(d) Sr	(e) Precipitate	(f) Others	Total <sup>a)</sup>
		Glass 44m <sup>2</sup> /piece	Glass 44m <sup>2</sup> /piece	Alloy 0.5m <sup>2</sup> /piece	Calcined 4.4m <sup>2</sup> /piece	Calcined 4.4m <sup>2</sup> /piece	Glass 2.5m <sup>2</sup> /piece	Glass 11m <sup>2</sup> /piece	
UO <sub>2</sub>	5 y	49.3	40.9	(1.04)	3.77	3.05	0.48	1.18	8.47 (9.51)
	10 y	49.1	37.0	(1.04)	3.60	3.14	0.48	1.18	8.40 (9.43)
	20 y	48.2	37.0	(1.04)	3.35	3.26	0.48	1.18	8.27 (9.30)
	50 y	51.9	37.1	(1.04)	2.87	3.49	0.48	1.18	8.02 (9.05)
MOX	5 y	99.4	36.4	(1.46)	4.09	2.89	0.44	1.10	8.52 (9.98)
	10 y	139.0	36.4	(1.46)	3.92	3.01	0.44	1.10	8.47 (9.93)
	20 y	193.2	36.5	(1.46)	3.66	3.18	0.44	1.10	8.39 (9.85)
	50 y	251.7	36.5	(1.46)	3.17	3.50	0.44	1.10	8.22 (9.68)

a) Areas in parentheses are including the areas for Tc-PGM group which may be reused or transmuted.

# The ADS Concept

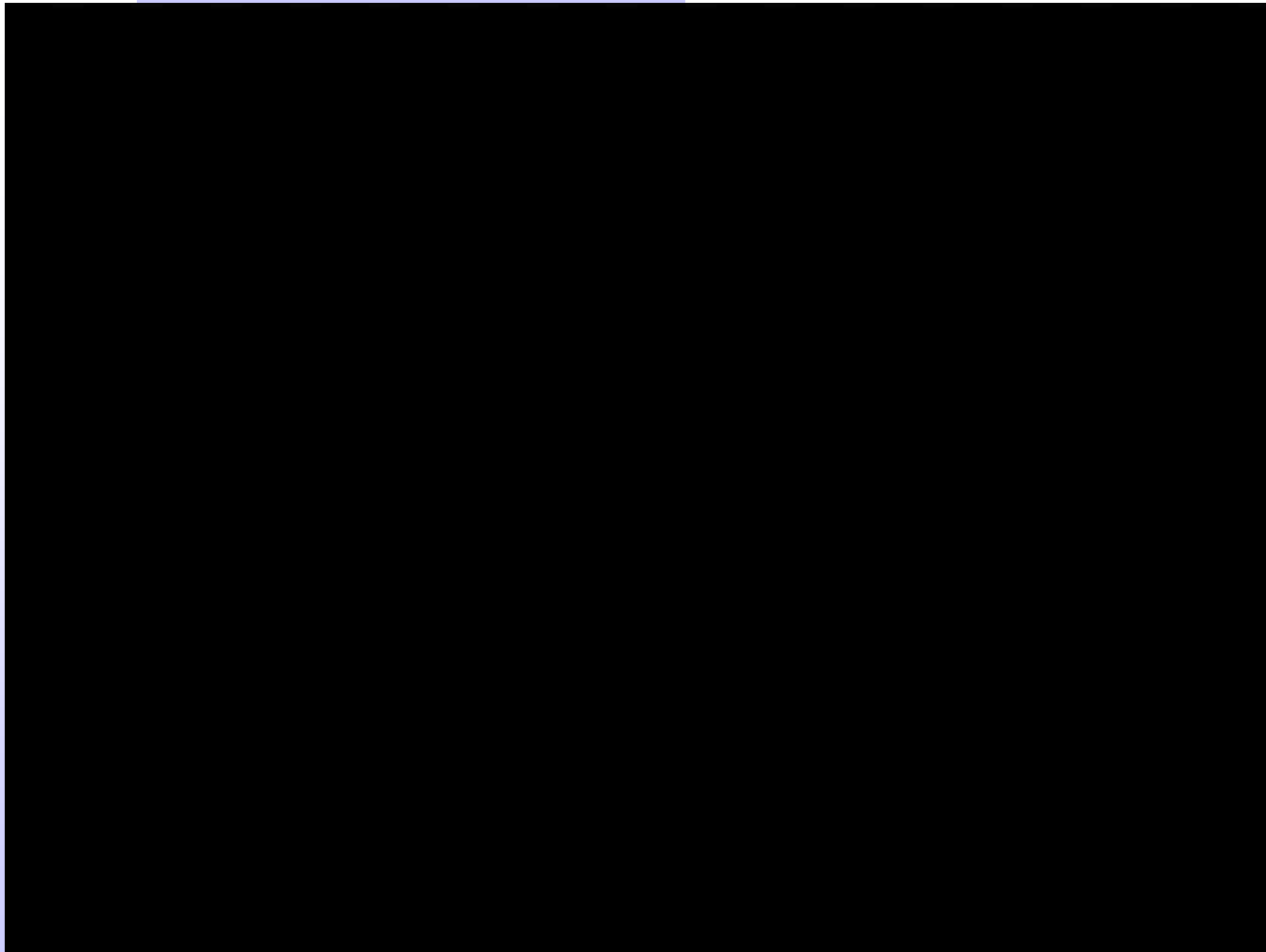


ADS systems are presently studied for nuclear waste transmutation because of the  $\beta$  (delayed neutron fraction which let the reactor control):

<sup>235</sup> U	650 pcm	<sup>238</sup> U	1480 pcm
<sup>238</sup> Pu	120 pcm	<sup>239</sup> Pu	210 pcm
<sup>240</sup> Pu	270 pcm	<sup>241</sup> Pu	490 pcm
<sup>242</sup> Pu	573 pcm	<sup>237</sup> Np	334 pcm
<sup>241</sup> Am	113 pcm	<sup>243</sup> Am	208 pcm
<sup>242</sup> Cm	33 pcm	<sup>244</sup> Cm	100 pcm

**Therefore if one wants to load large quantities of MAs in the Waste burner it should be a subcritical machine**

# The ADS Principle



- SCK•CEN core competencies: design, realisation and operation of large nuclear research facilities (BR1, BR2, BR3, VENUS reactors, Pu-Lab, LHMA Hot cells, HADES URL for waste Mgt).
- BR2, a 100 MW MTR, will soon be 45 years old, like other major MTRs in Europe (OSIRIS, HFR, R2).
- SCK•CEN and IBA have been associated to develop the ADONIS project during the 1995-97 period. ADONIS was a ~1.5 MW ADS with 0.15 to 0.3 MW low energy proton beam power (1 to 2 mA \* 150 MeV) for Radioisotopes production

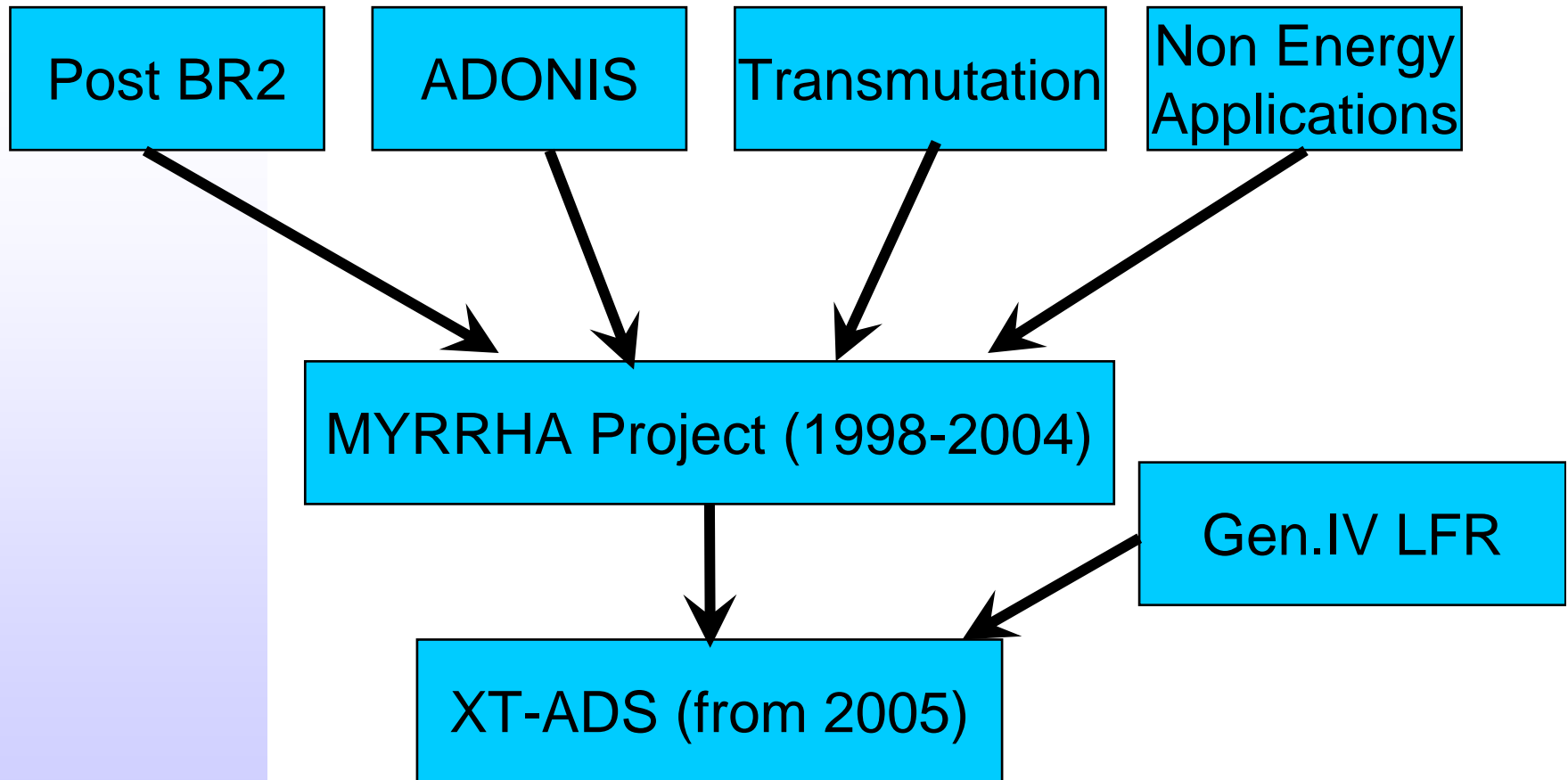
# MYRRHA in a European scene

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- the RJH (F) project, a **thermal** spectrum MTR, is the only planned testing reactor for the moment
- MYRRHA would be the natural **fast spectrum** complementary facility.
- This will put Europe in a strong position towards the support of Gen. III and development of Gen. IV reactors.

# MYRRHA Genesis & Evolution towards XT-ADS





# The Applications catalogue: MYRRHA/XT-ADS is to be:



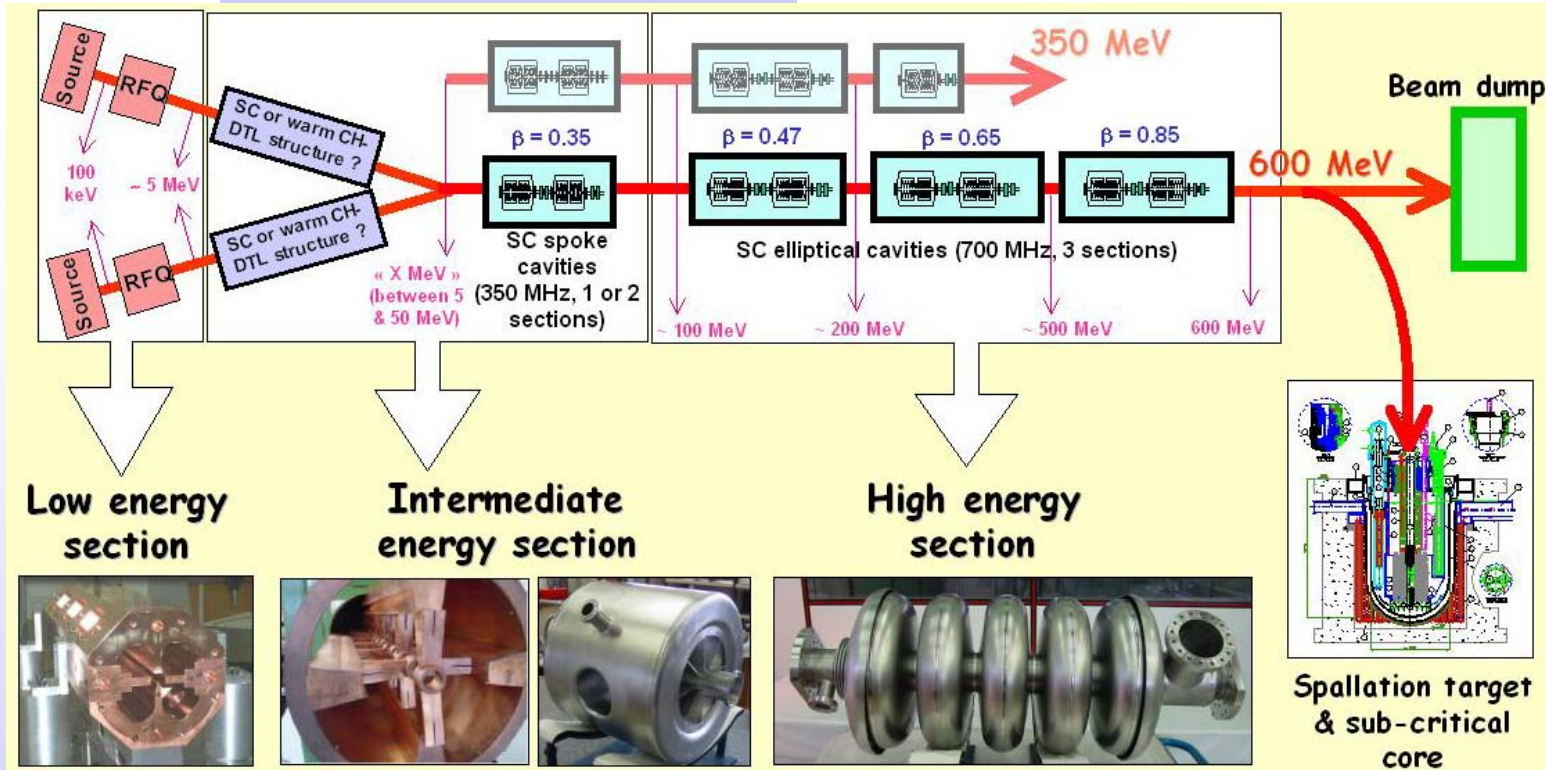
- A full step ADS demo facility
- A P&T testing facility
- A flexible irradiation testing facility in replacement of the SCK•CEN MTR BR2 (100 MW)
- An attractive fast spectrum testing facility in Europe, beyond 2015 complementary to RJH (F)
- HLM Technological prototype as test bench for LFR
- An attractive tool for education and training of young scientists and engineers
- A medical radioisotope production facility

# MYRRHA/XT-ADS Components



- ACCELERATOR
- SPALLATION SOURCE
- SUB-CRITICAL REACTOR
- REMOTE HANDLING & IN-SERVICE INSPECTION

# MYRRHA/XT-ADS Accelerator: the LINAC solution



Strong R&D & construction programs for SC linacs are underway worldwide for many applications (Spallation Sources for Neutron Science, Radioactive Ions & Neutrino Beam Facilities, Irradiation Facilities)

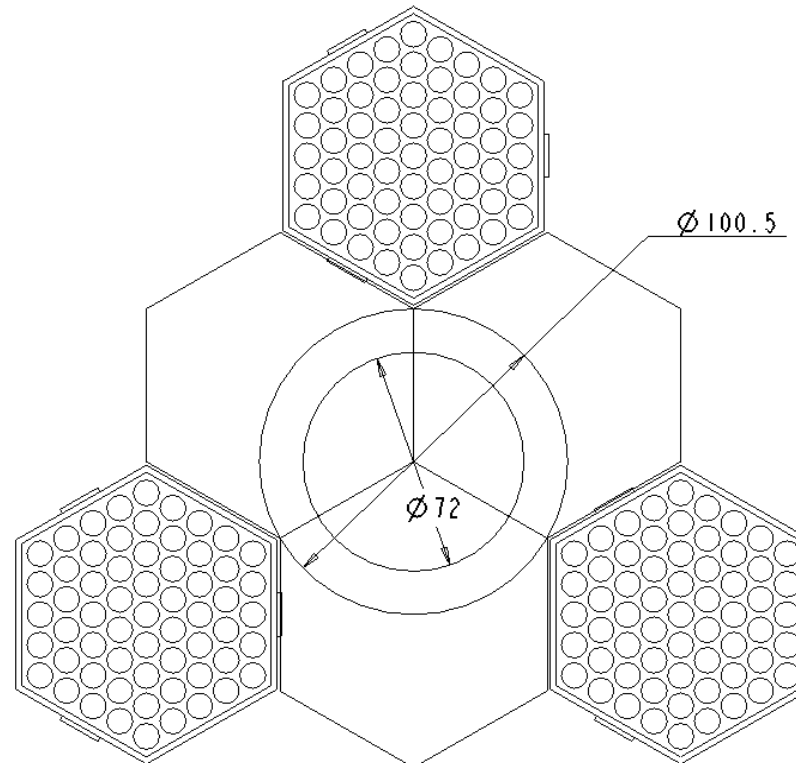
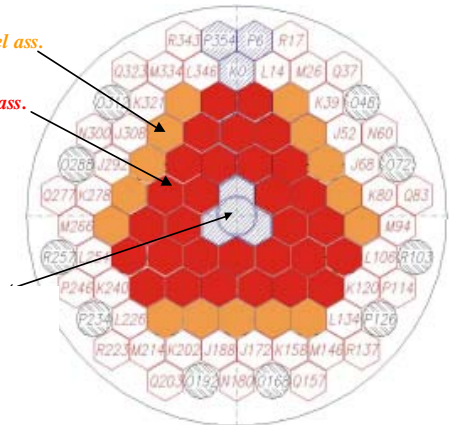
# Spallation Target: Radial Geometrical Constraints



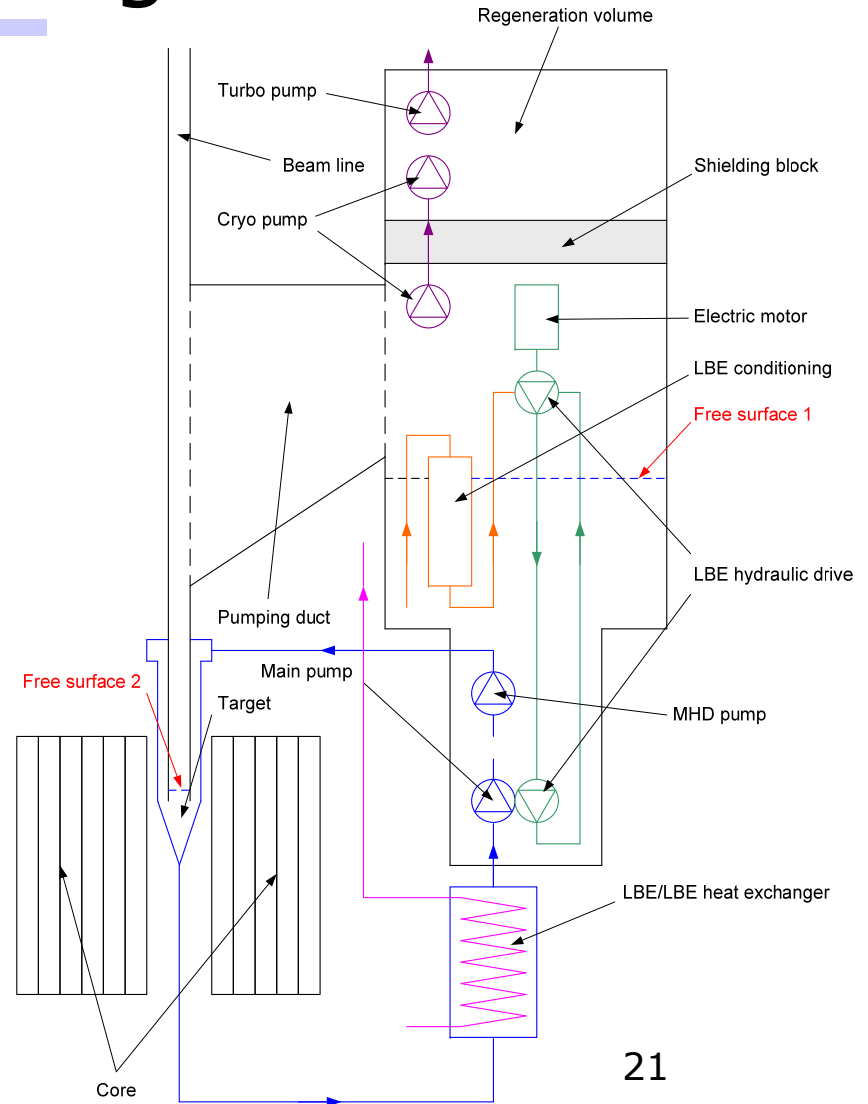
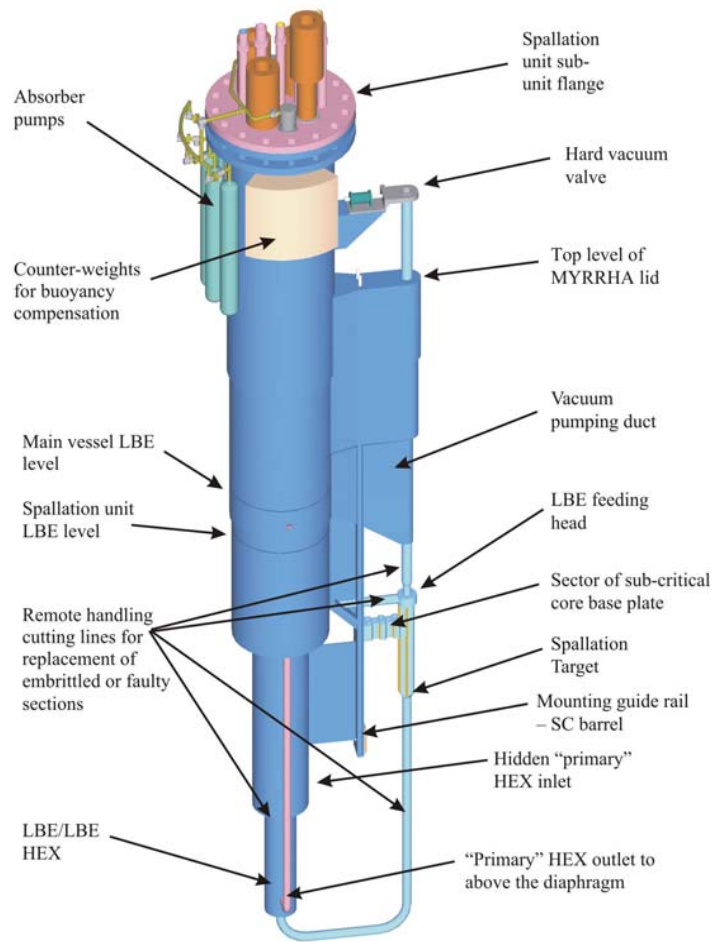
- Due to the high performances desired in the core, we limited drastically the central hole in the core for housing the spallation source

MOX-20% fuel ass.

MOX-30% fuel ass.



# MYRRHA/XT-ADS Spallation Target



# Sub-Critical Reactor

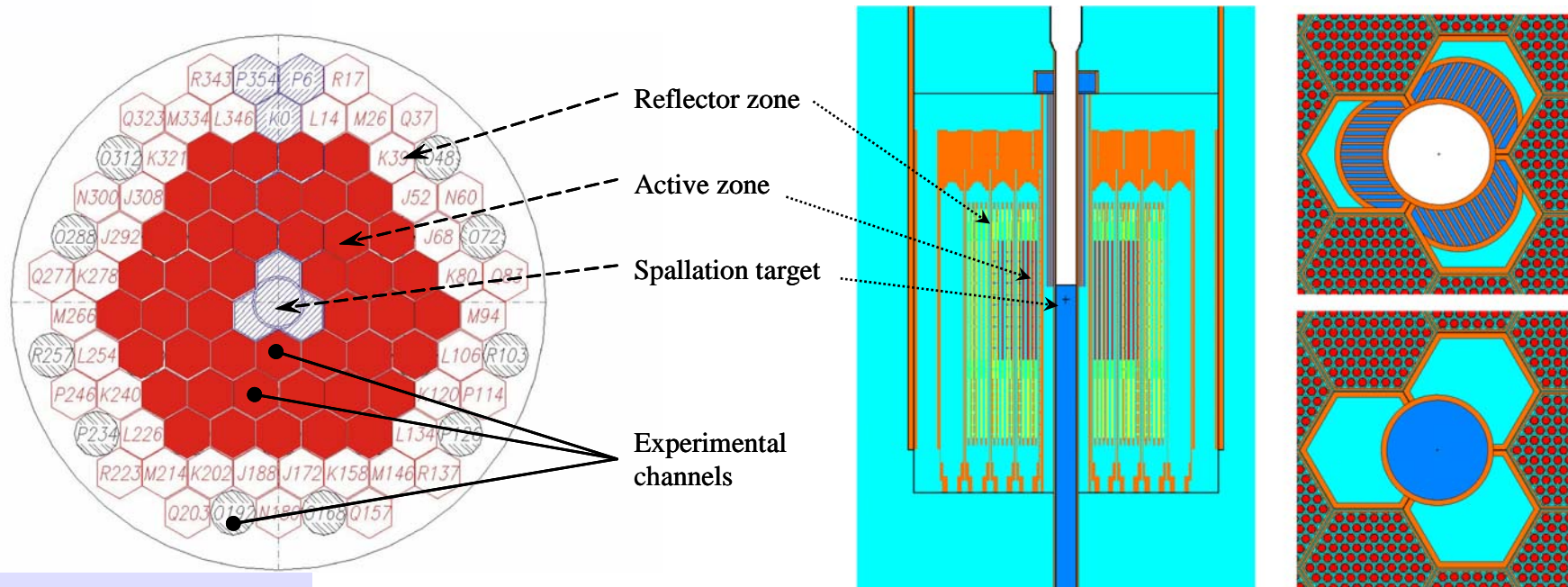
## Pb-Bi: benefits and drawbacks



- ☺ Undergoes spallation
- ☺ Reasonable melting temperature (123 °C)
- ☺ Water can be used for the secondary cooling
- ☹ High coolant density (steel and fuel float)
- ☹ Opaque: blind fuel handling
- ☹ Possible problems in case of variation of the eutectic composition (deposits of high melting point phases)
- ☹ Bi activates into Po
- ☹ The compatibility of Pb-Bi with structural and cladding materials is to be addressed by design

# MYRRHA Core configuration

## Under updating for XT-ADS

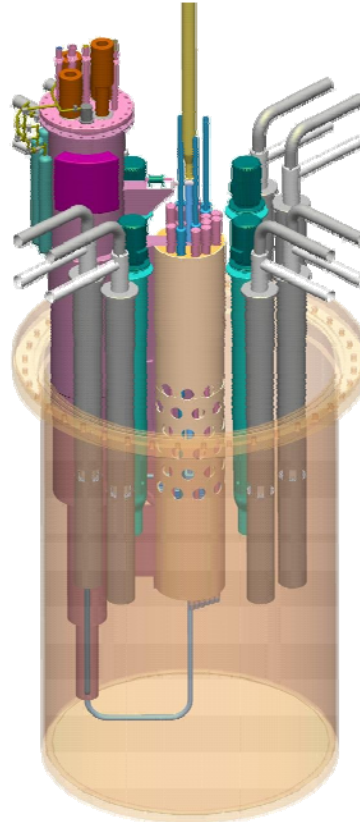


- 99 + 3 hexagonal cells (“macro-cells”)
- Target-block hole is made by 3 removed FA in the central region
- Surrounding active zone composed of 45 (or more) FA
- Outer reflector zone composed of 54 (or less) reflector assemblies

## MYRRHA design description Primary cooling system



- The cooling system is *designed* for  $60 \text{ MW}_{th}$
- The total heat production in the vessel is the sum of the nominal *core* heat production ( $50 \text{ MW}_{th}$ ) and *other* heat sources (1.8 MW)
- Two options were studied : pressurized and boiling water heat exchangers



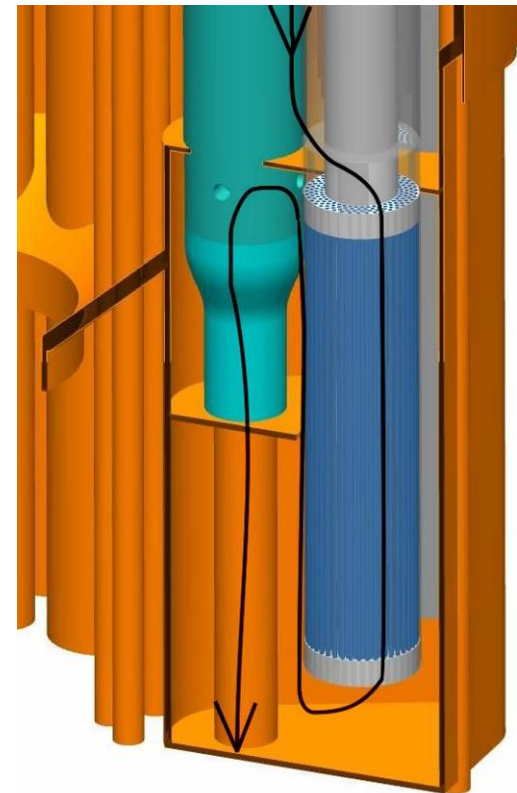
- *Four groups* with each one pump and two LBE/water heat exchangers are installed at the periphery of the vessel = 4 pumps and 8 heat exchangers.
- The system is *capable* to evacuate the total heat production even in the case of the *failure of one pump*



## MYRRHA design description Primary cooling system



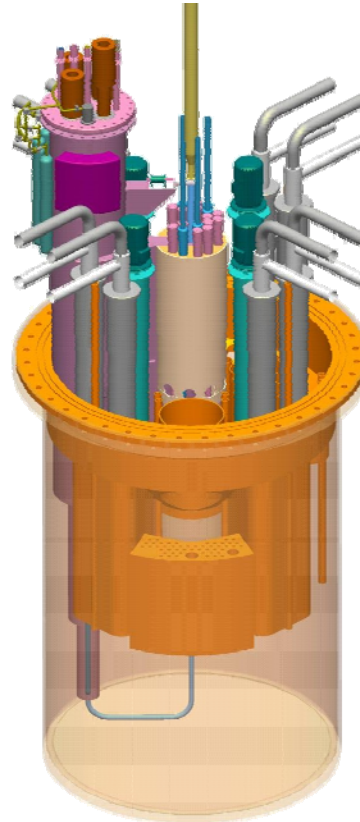
- Each HX/PP group is placed in its casing in such a way that the flow path describes a vertical *chicane* which should help to *avoid water ingress* in the core by providing the separation of water/ vapour and Pb-Bi in case of a tube rupture.
- A *leak detection system* on each HX/pump casing is foreseen. It detects the presence of steam or water at the high point of the chicane.



## MYRRHA design description Diaphragm

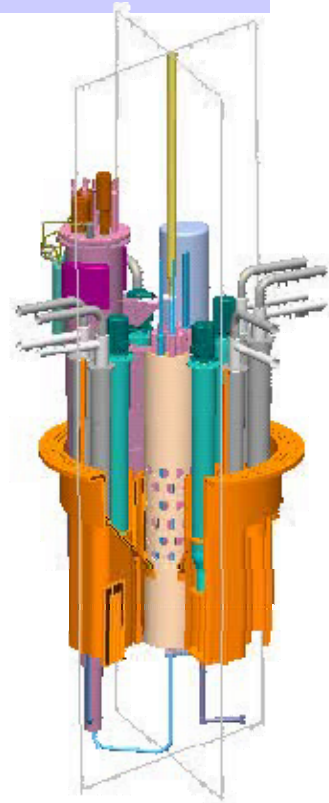


- forces the coolant *flow path* through the core, separating the lower part (200°C, high pressure) of the Pb-Bi from the upper part (337°C, low pressure);
- supports the two in-vessel *fuel storages* (which are foreseen to avoid excessive delay between operation cycles);



- has *4 casings* containing the pumps and heat exchangers;
- has numerous *penetrations* for the large components (spallation loop, core, pumps, heat exchangers, handling machines) and for the smaller irradiation devices.

# MYRRHA design description Diaphragm

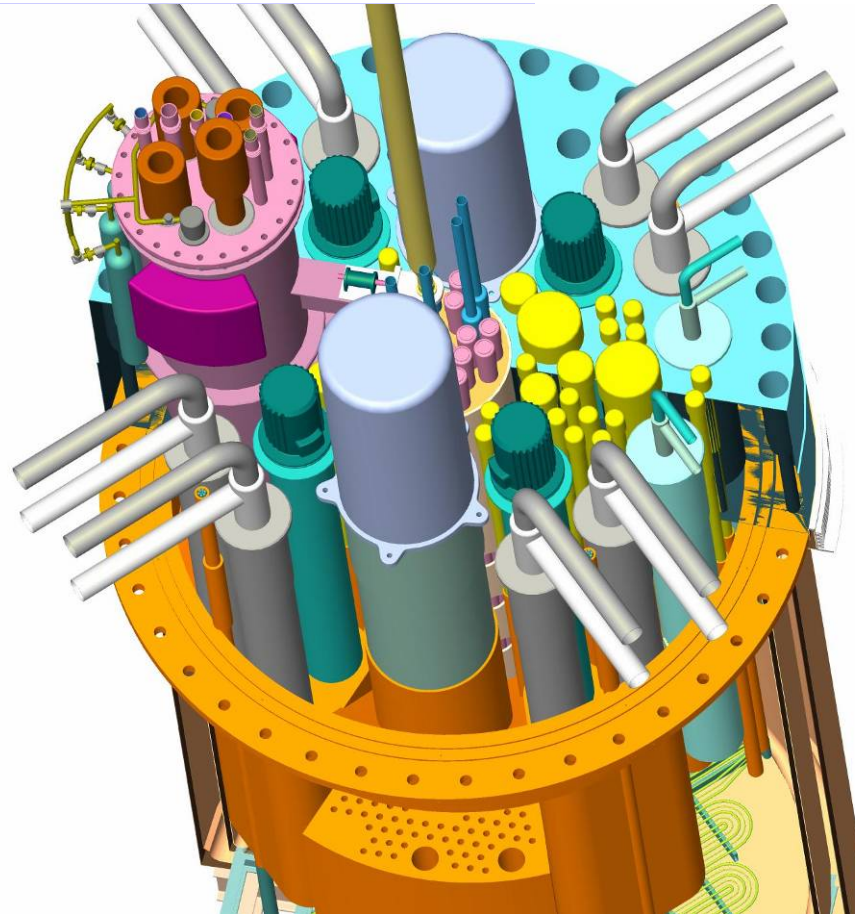


## MYRRHA design description In-vessel fuel manipulators

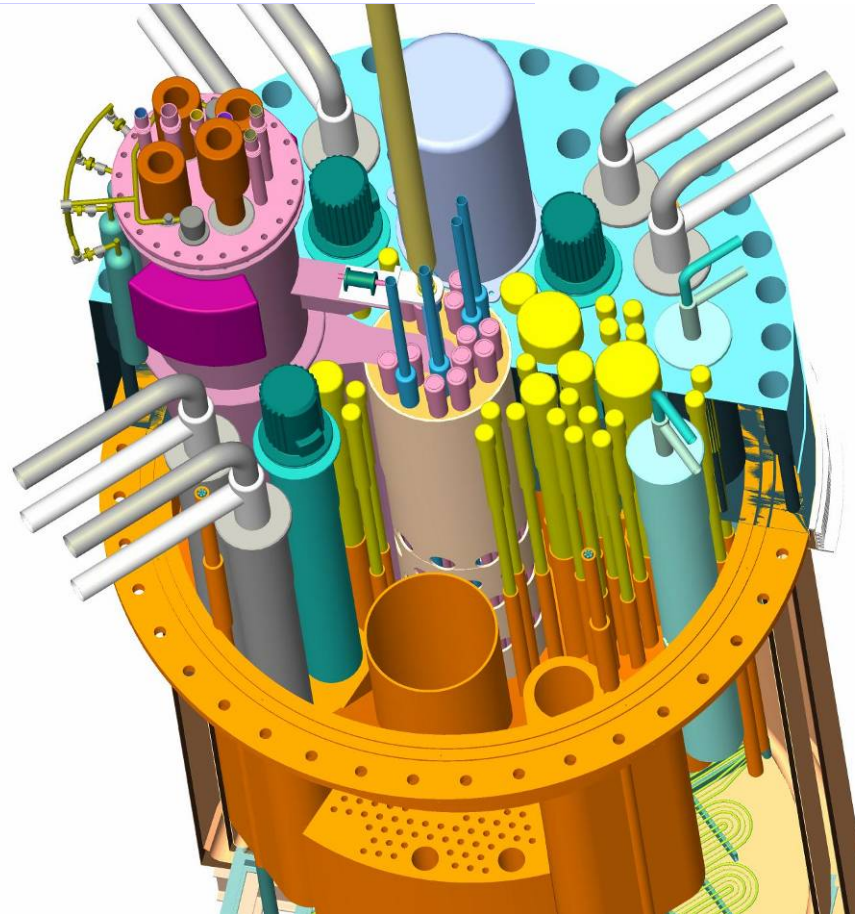


- The fuel handling is performed *underneath* the core:
  - because the *irradiation devices* (inside the core and in the periphery of the core as well) will stay several cycles in the reactor and because their handling will be a difficult process, it is wished to keep them into location while reloading the core – this makes fuel manipulation above the core very impractically;
  - the room situated directly above the compact core will be *occupied* by instrumentation, the beam tube and partially by the spallation loop, with which the fuel handling would interfere if performed from the top of the core,
  - the *interlinking* of the spallation loop with the core makes some fuel assembly positions inaccessible from above,
- The fuel assemblies rest by *buoyancy* force under the support plate.

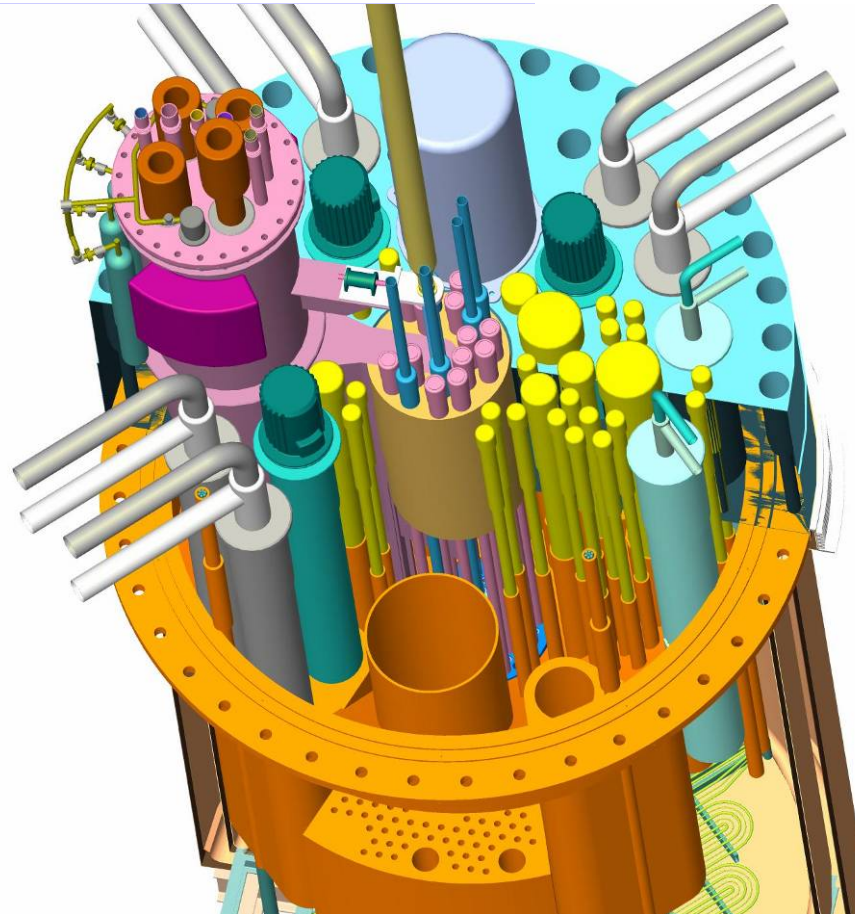
# MYRRHA design description In-vessel fuel manipulators



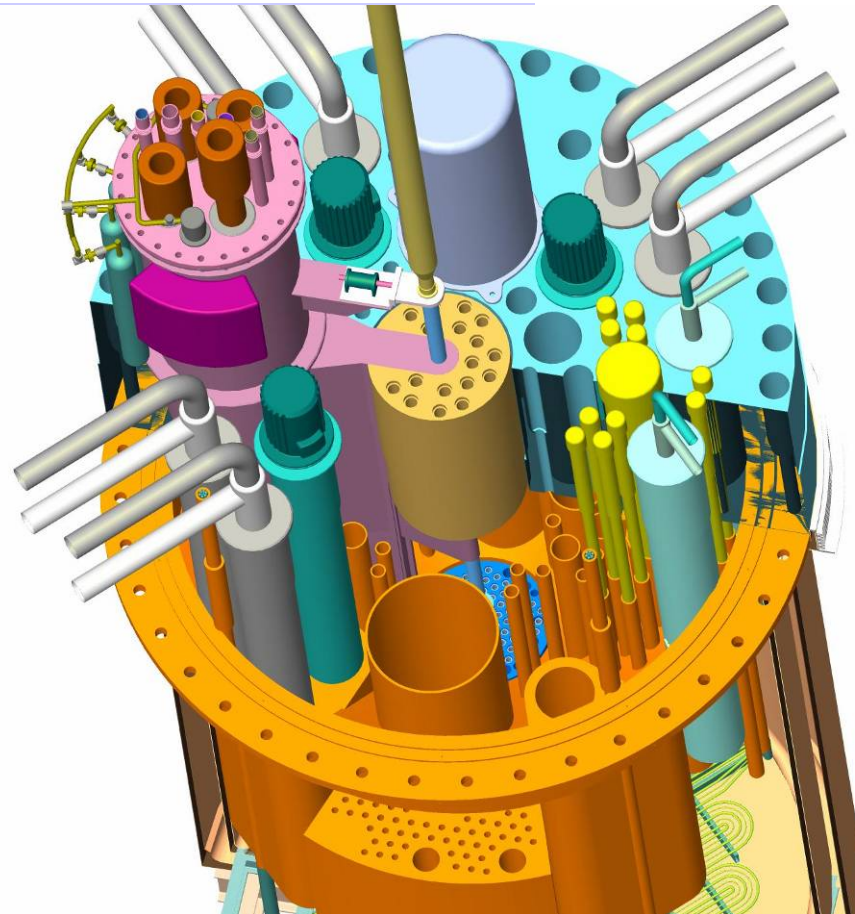
# MYRRHA design description In-vessel fuel manipulators



# MYRRHA design description In-vessel fuel manipulators

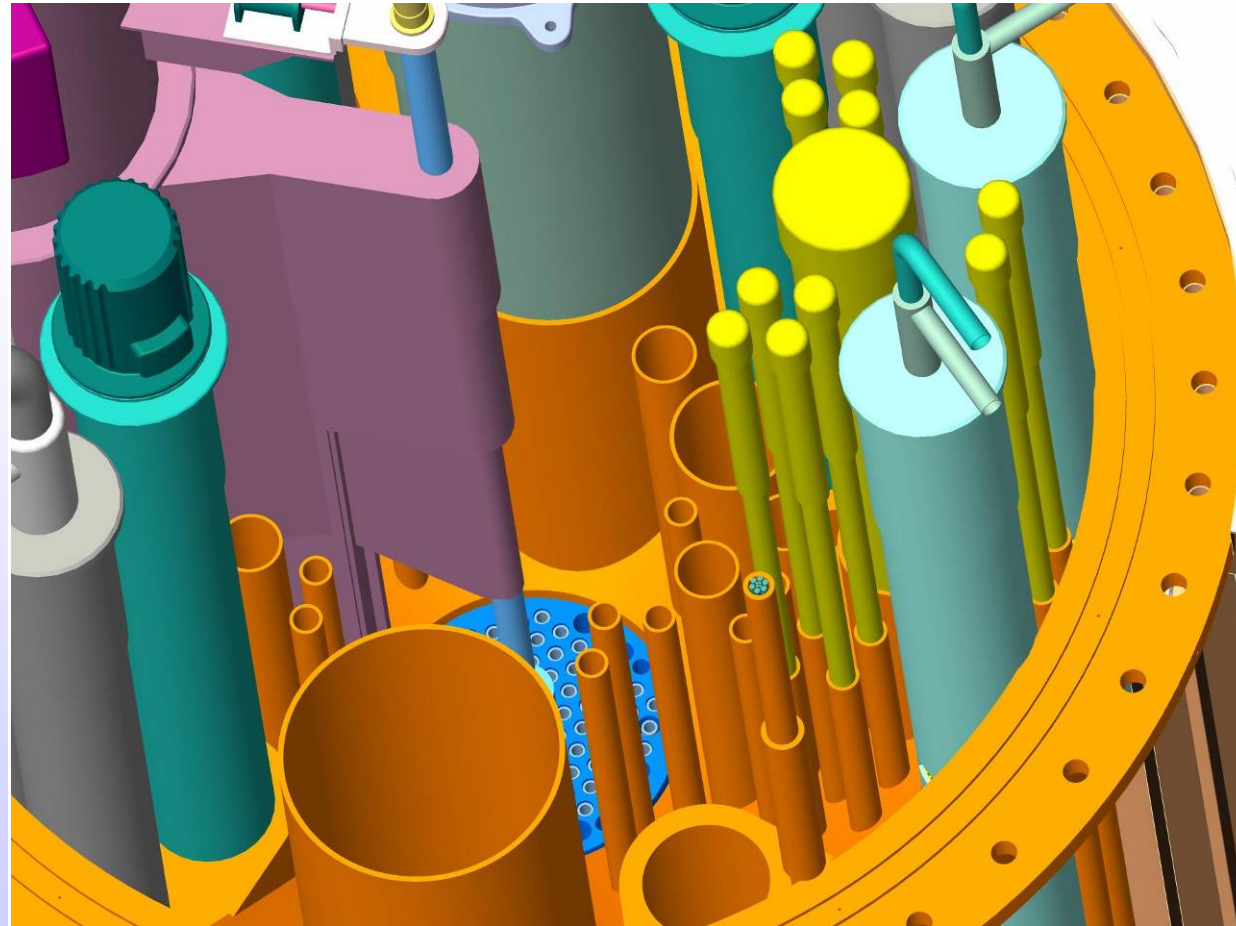


# MYRRHA design description In-vessel fuel manipulators



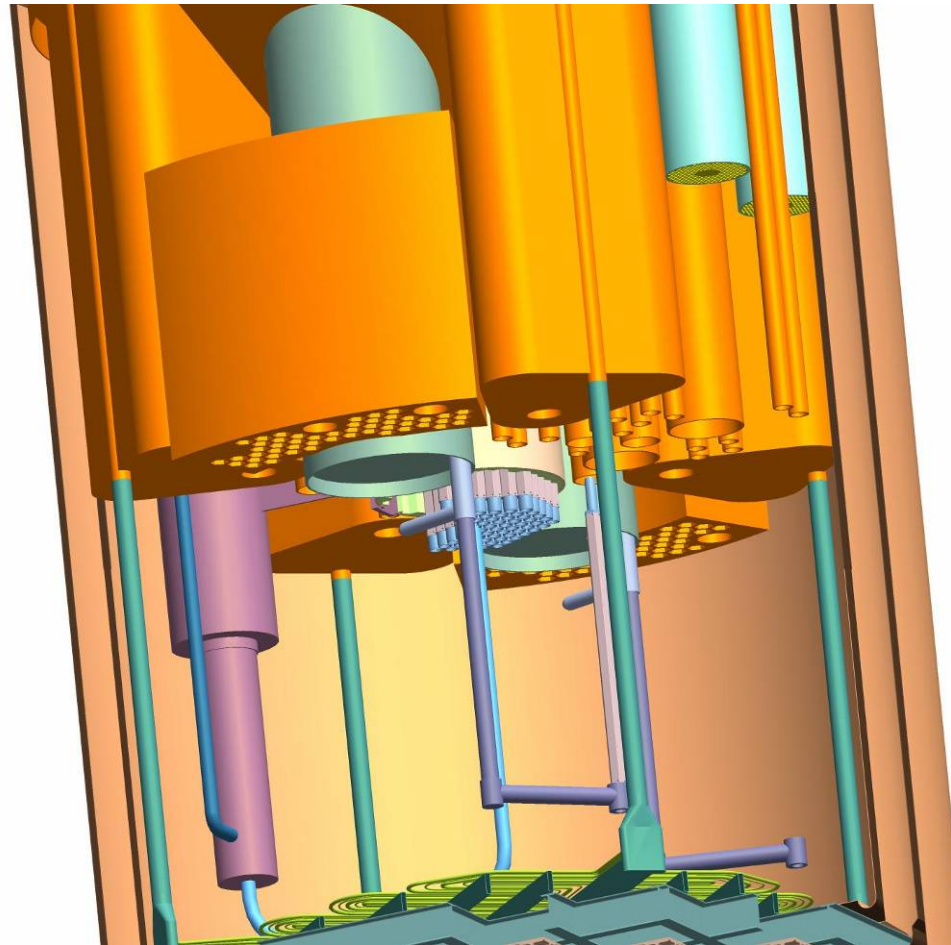


# MYRRHA design description In-vessel fuel manipulators



# MYRRHA design description

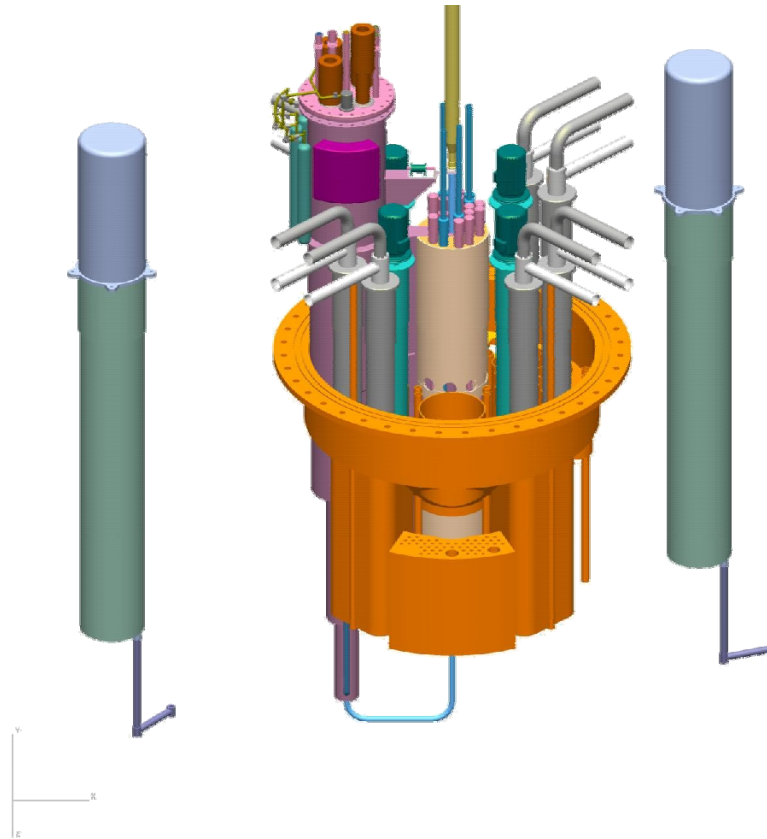
## In-vessel fuel manipulators



### 3. MYRRHA design description In-vessel fuel manipulators

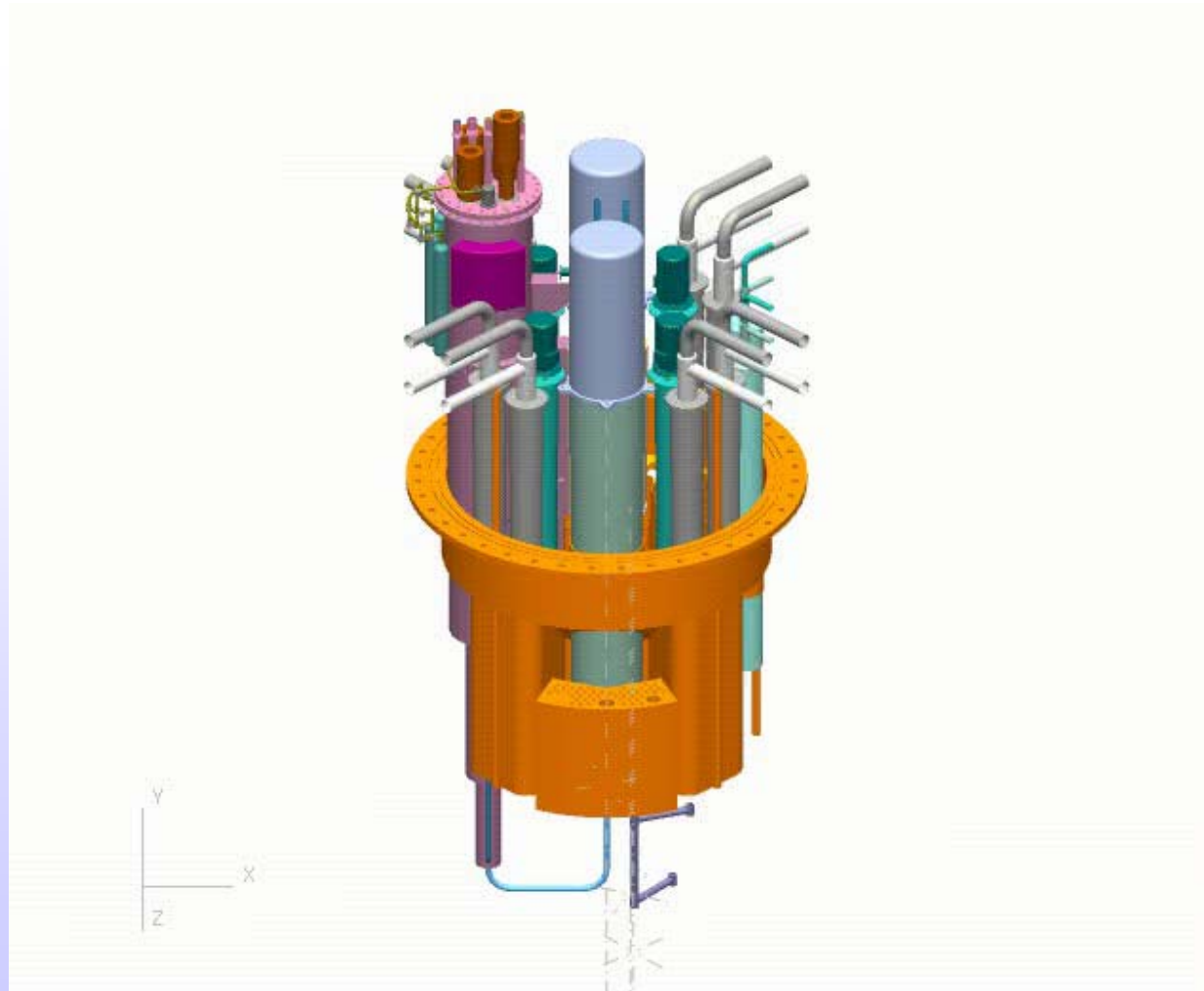
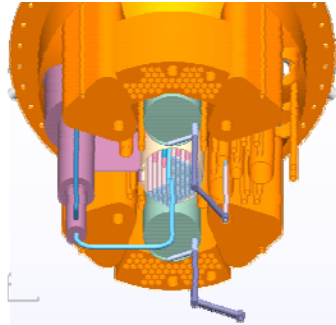


- *Two* handling systems are inserted in a penetration of the reactor cover on opposite sides of the core.
- Each system has a *rotating plug*, with an *offset arm*.



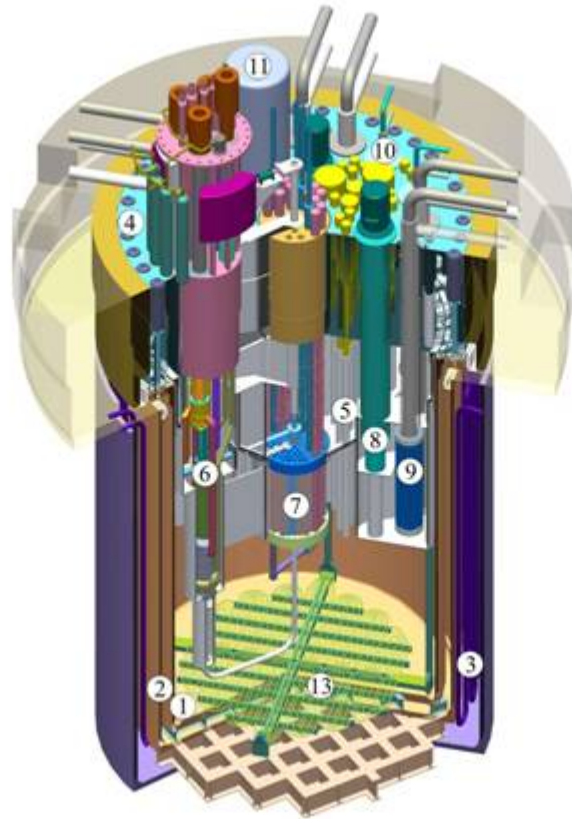
- The arm can rotate in the rotating plug, and so has *access to half of the core*.
- The arm can move up and down by about 2 m to extract the assemblies from the core.

# MYRRHA design description In-vessel fuel manipulators



# Design of MYRRHA Overall configuration

## Under updating for XT-ADS



1. inner vessel
2. guard vessel
3. cooling tubes
4. cover
5. diaphragm
6. spallation loop
7. sub-critical core
8. primary pumps
9. primary heat exchangers
10. emergency heat exchangers
11. in-vessel fuel transfer machine
12. in-vessel fuel storage
13. coolant conditioning system

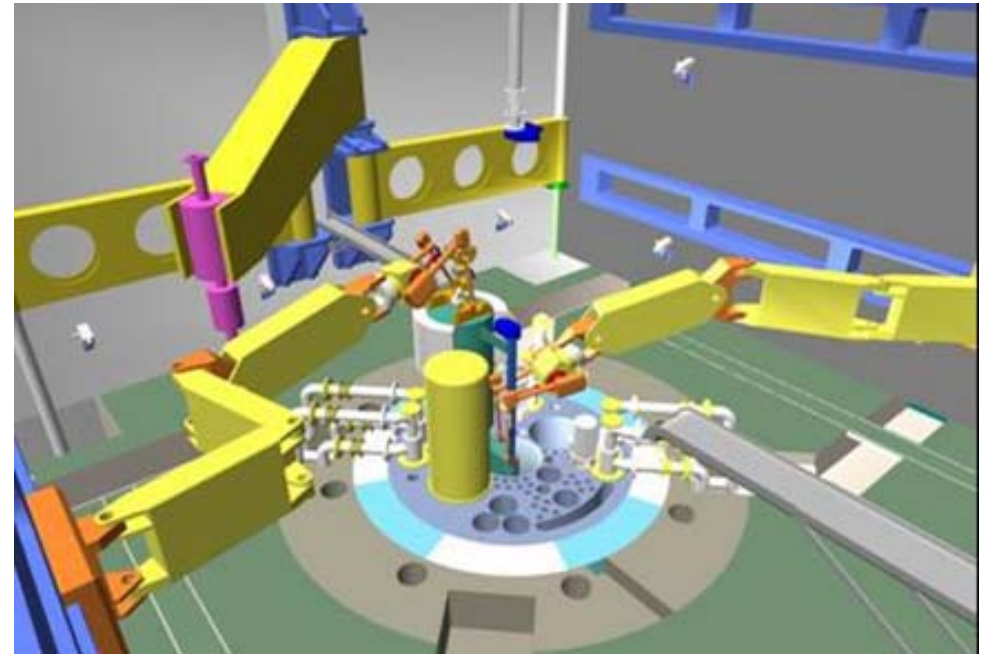


# Design of MYRRHA: Remote handling



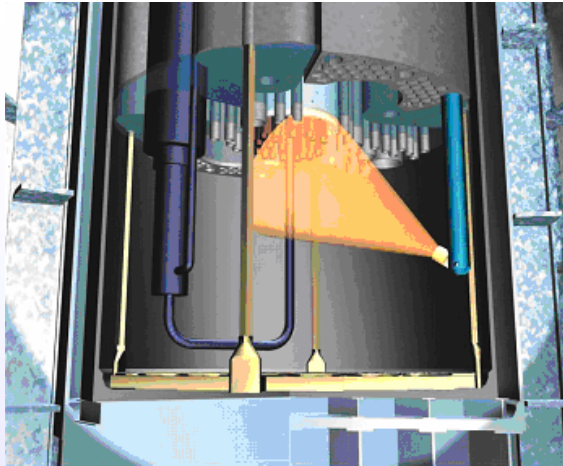
All MYRRHA maintenance & operation on the machine primary systems and associated equipment are performed by remote handling, which is based on the *Man-In-The-Loop principle*:

- force reflecting servomanipulators
- Master-Slave mode: the slave servo-manipulators are commanded by remote operators using kinematically identical master manipulators
- supported with closed-cycle TV (CCTV) feedback

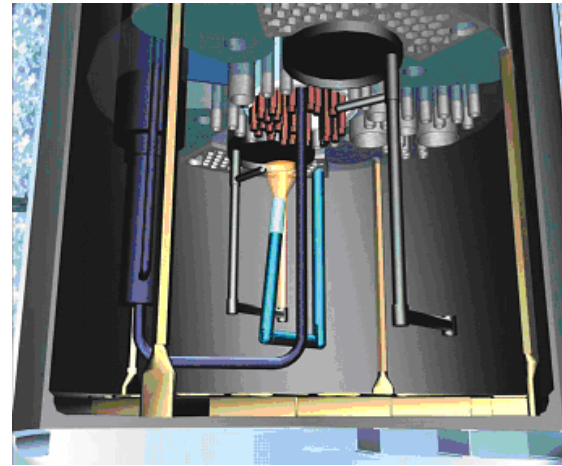


OTL concludes positive on the feasibility of the proposed RH approach.

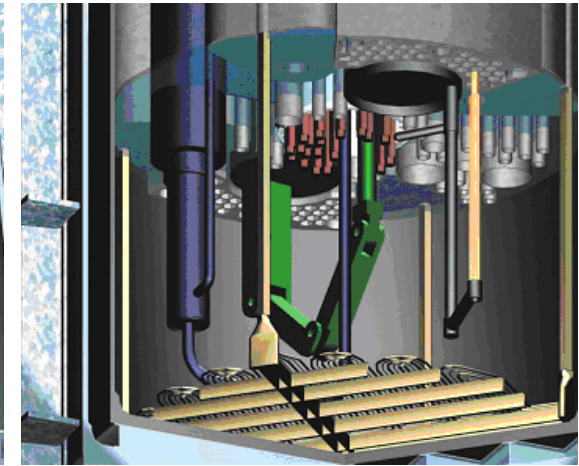
# Design of MYRRHA: In-service inspection and repair



Two permanently installed *inspection* manipulators with US camera to provide a general *overview*. (periscope type device with three degrees of freedom)



The second *inspection* manipulator positions the camera close to critical components for *detailed* inspection. (anthropomorphic type device with five degrees of freedom)



The *repair* manipulator recovers debris or deploys specialised tooling for repair. (anthropomorphic type device with eight degrees of freedom)

OTL concludes positive on the feasibility of the proposed RH approach.

# Perspectives for Implementation



# 1-SCK•CEN Commitment



- SCK•CEN Mgt has declared its readiness to welcome a fast spectrum irradiation facility at its technical site in Mol
- SCK•CEN has finished the preparation of a business plan and a funding plan that has been made available to the Belgian Government in May 2007 and will be presented to potential partners by autumn 2007
- Bilateral discussions with some potential partners are already going on (CNRS, CEA, CIEMAT, ...)

## 2-Opening MYRRHA to Europe => XT-ADS



- MYRRHA Draft-2 has been made available to the EUROTRANS Community
- SCK•CEN is studying in collaboration with EUROTRANS partners the modifications needed to achieve the XT-ADS objectives
- Considering Joint Undertaking for setting up the frame for the realisation at European level

## 2. XT-ADS design description Reference architecture



- The reference architecture of the **primary system** as decided during Eurotrans DCC\_2 meeting (Lyon 10/2006):
- **Modifications** with respect to MYRRHA (*between brackets*)
  - primary system capable to extract **70 MW<sub>th</sub>** total heat power (*60 MW<sub>th</sub>*)
  - core inlet and outlet LBE cooling temperatures : **300°C – 400°C** (*200°C – 340°C*)
  - improved natural convection in case of PLOH by:
    - ✓ core pressure drop **Δp limited to 1000 mbar**
    - ✓ increased elevation between **PHX & core to 2 m**
  - simplified **flat** diaphragm
  - reduced number of primary components to **2 groups** to reduce costs (*4 groups*)

## 2. XT-ADS design description Reference architecture

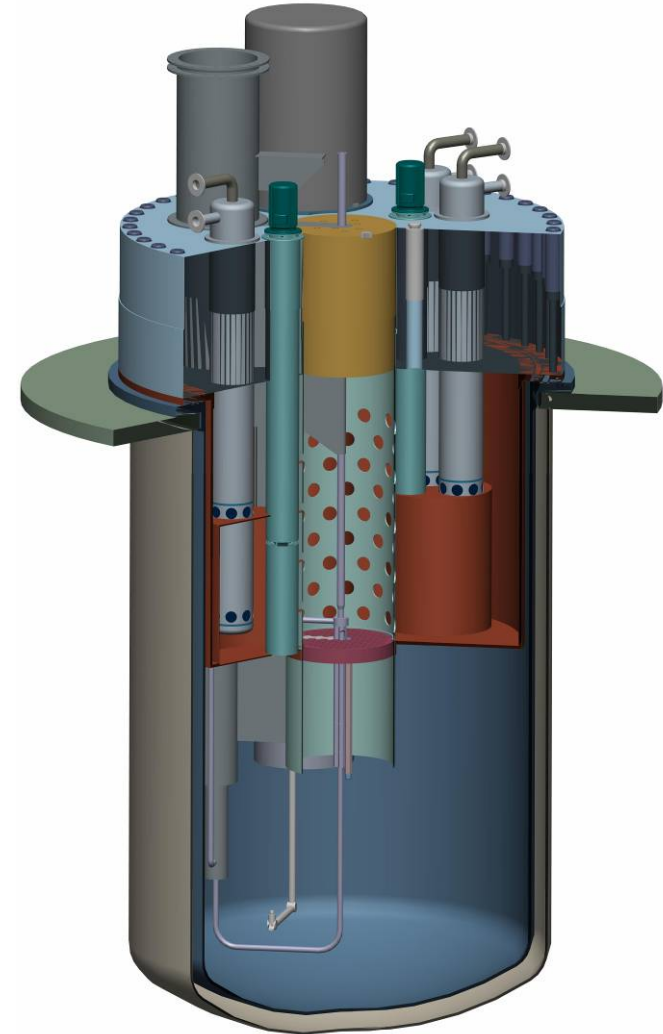
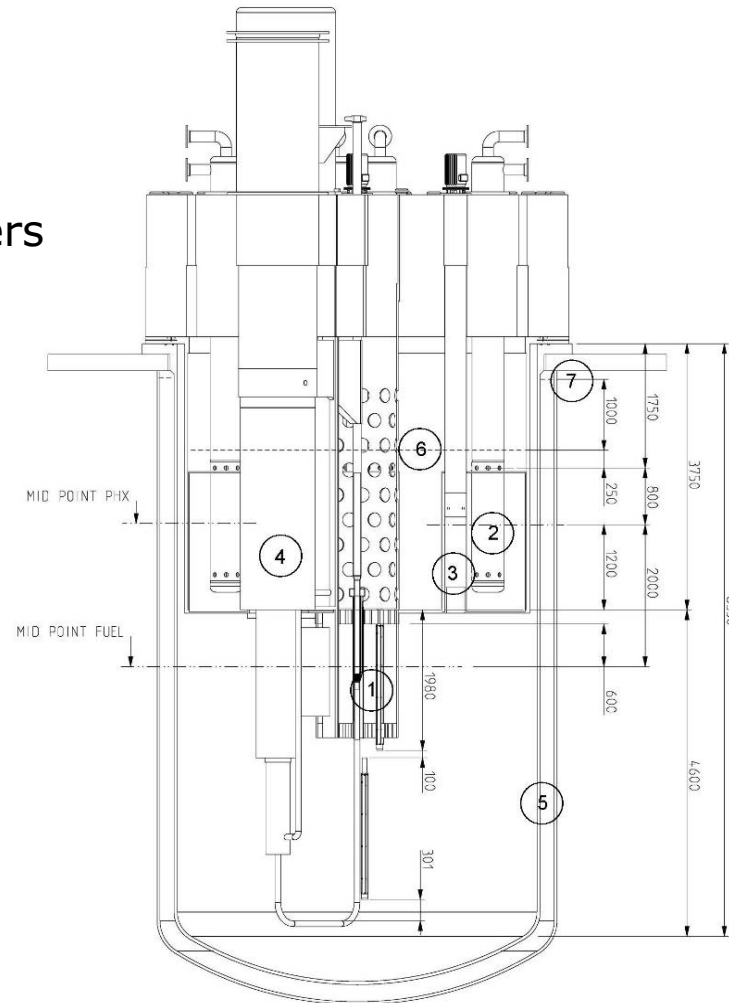


- Modifications with respect to MYRRHA (cont'd)
  - reduced number of possible IPS in the core to **8** possible positions  
*(19 positions)*
  - no test rigs positions outside the core  
*(many positions outside the core)*
  - **boiling** water heat exchangers at lowest possible pressure
  - decay heat removal (**DHR**) through PHX/secondary loops + vault cooling system (RVACS)  
*(emergency heat exchangers)*
  - **hanging** vessel with **elliptical** bottom head  
*(standing vessel with flat bottom)*
  - LBE cold plenum has free level (0.5 m underneath vessel top)
  - LBE hot free level is 1 m underneath cold free level (=  $\Delta p$  core)

## 2. XT-ADS design description

### XT-ADS overall configuration

1. Core
2. Heat exchangers (2 x 2)
3. Pumps (2 x 1)
4. Spallation loop
5. Vessels
6. LBE hot level
7. LBE cold level

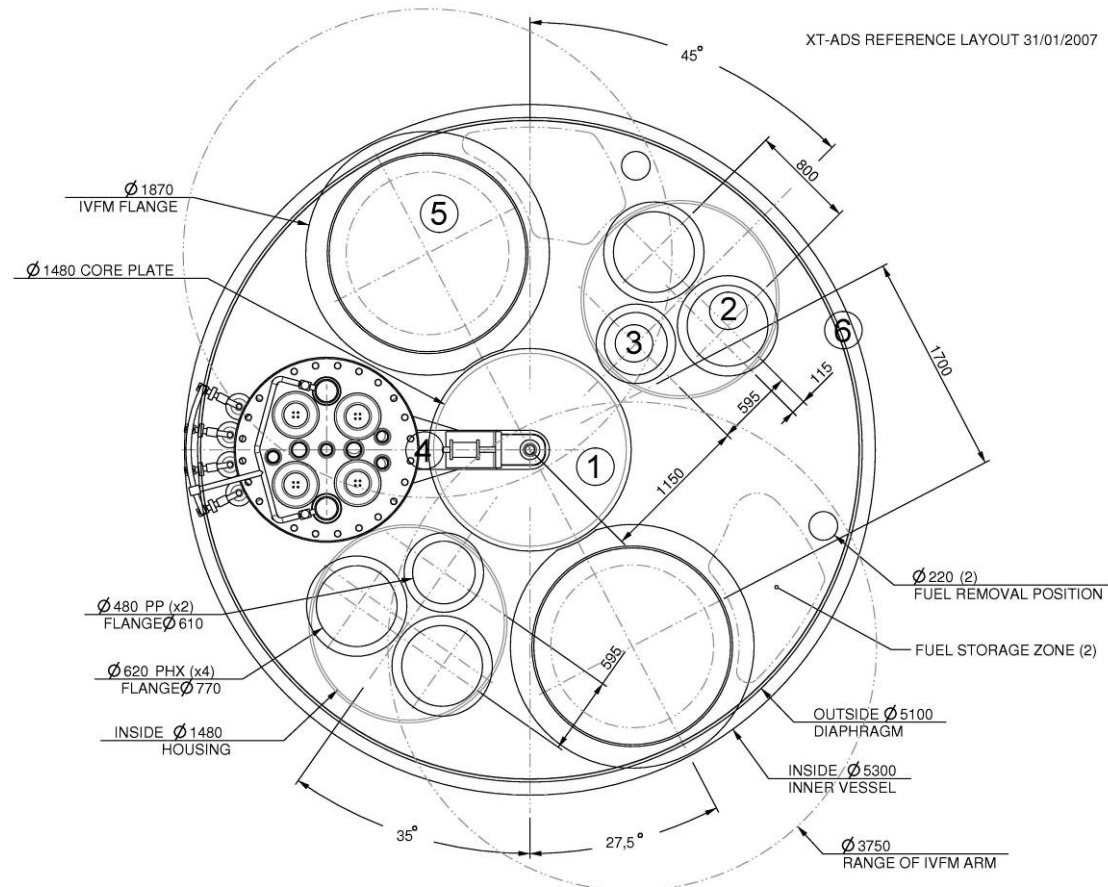


## 2. XT-ADS design description

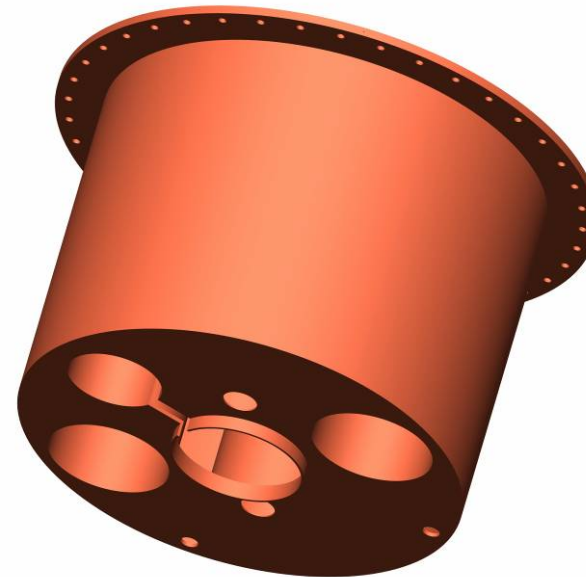
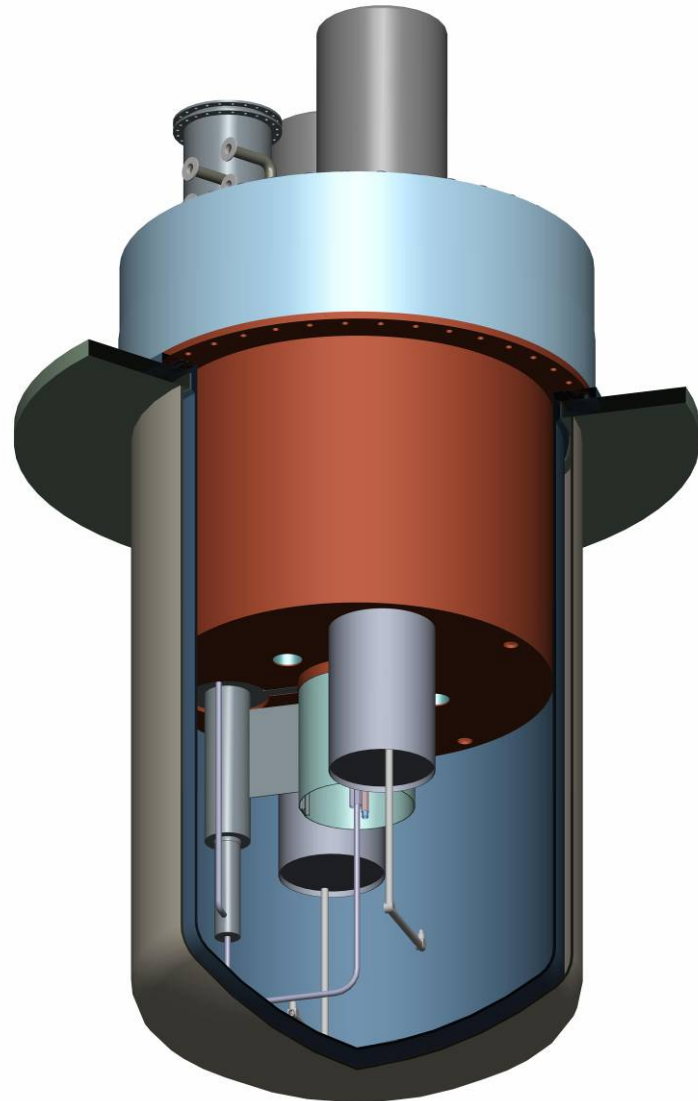
### XT-ADS overall configuration



1. Core
2. Heat exchangers (2 x 2)
3. Pumps (2 x 1)
4. Spallation loop
5. Fuel manipulators (2 units)
6. Vessel

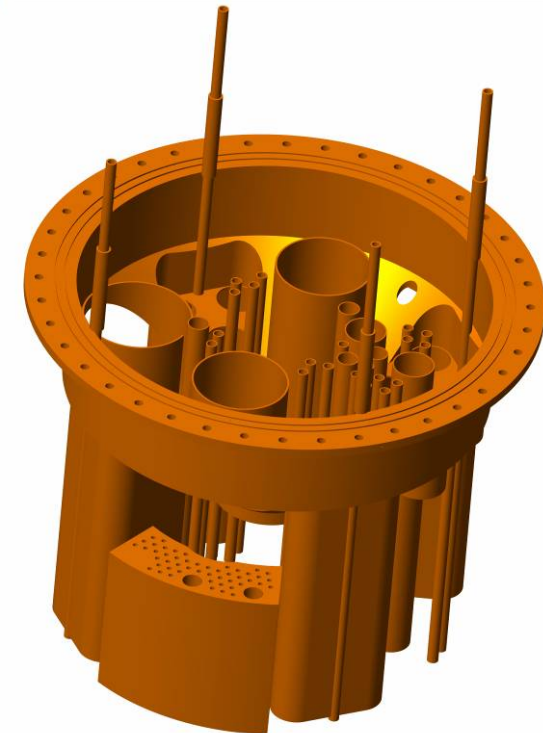


## 2. XT-ADS design description Simplified diaphragm



XT-ADS

MYRRHA



### 3. Holding the objective of Fast irradiation facility

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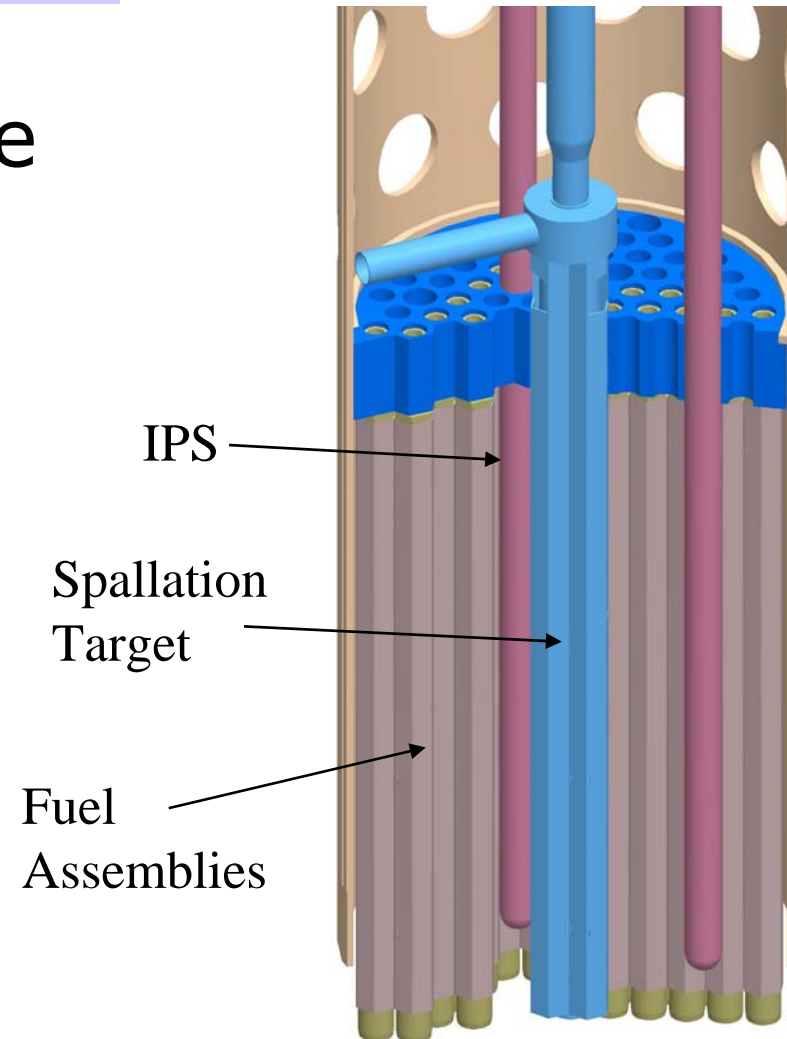
- Multi-irradiation channels available
- High performance levels
- Multiple irradiation conditions secured to the user



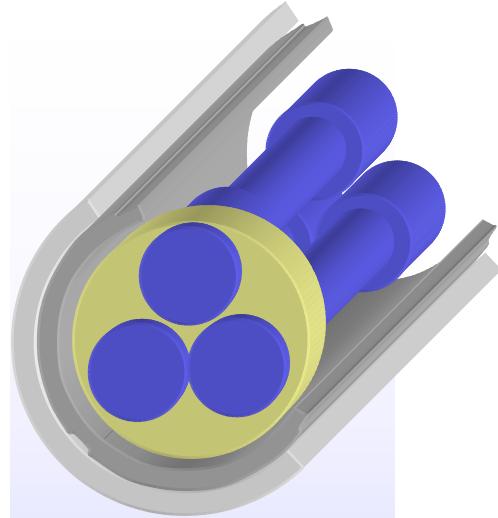
# 3. Material Irradiation in MYRRHA



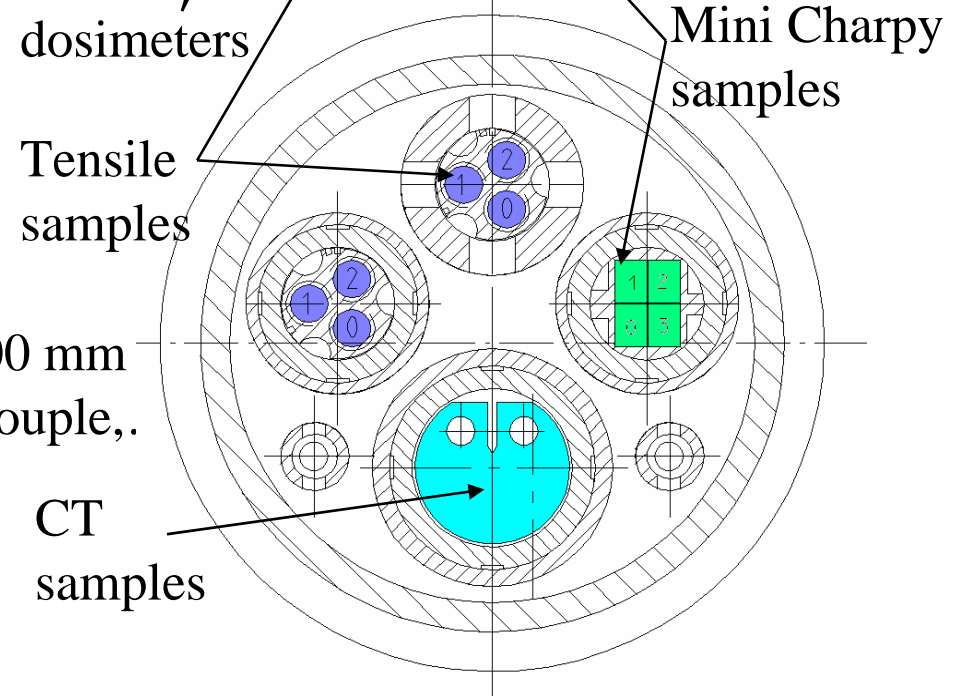
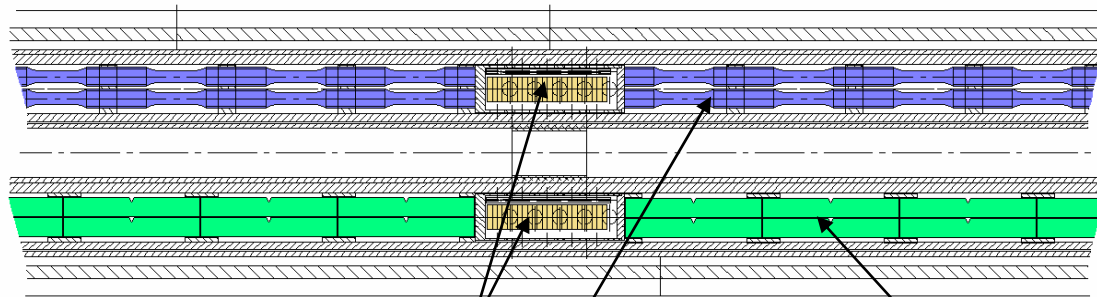
- IPS Location in the core



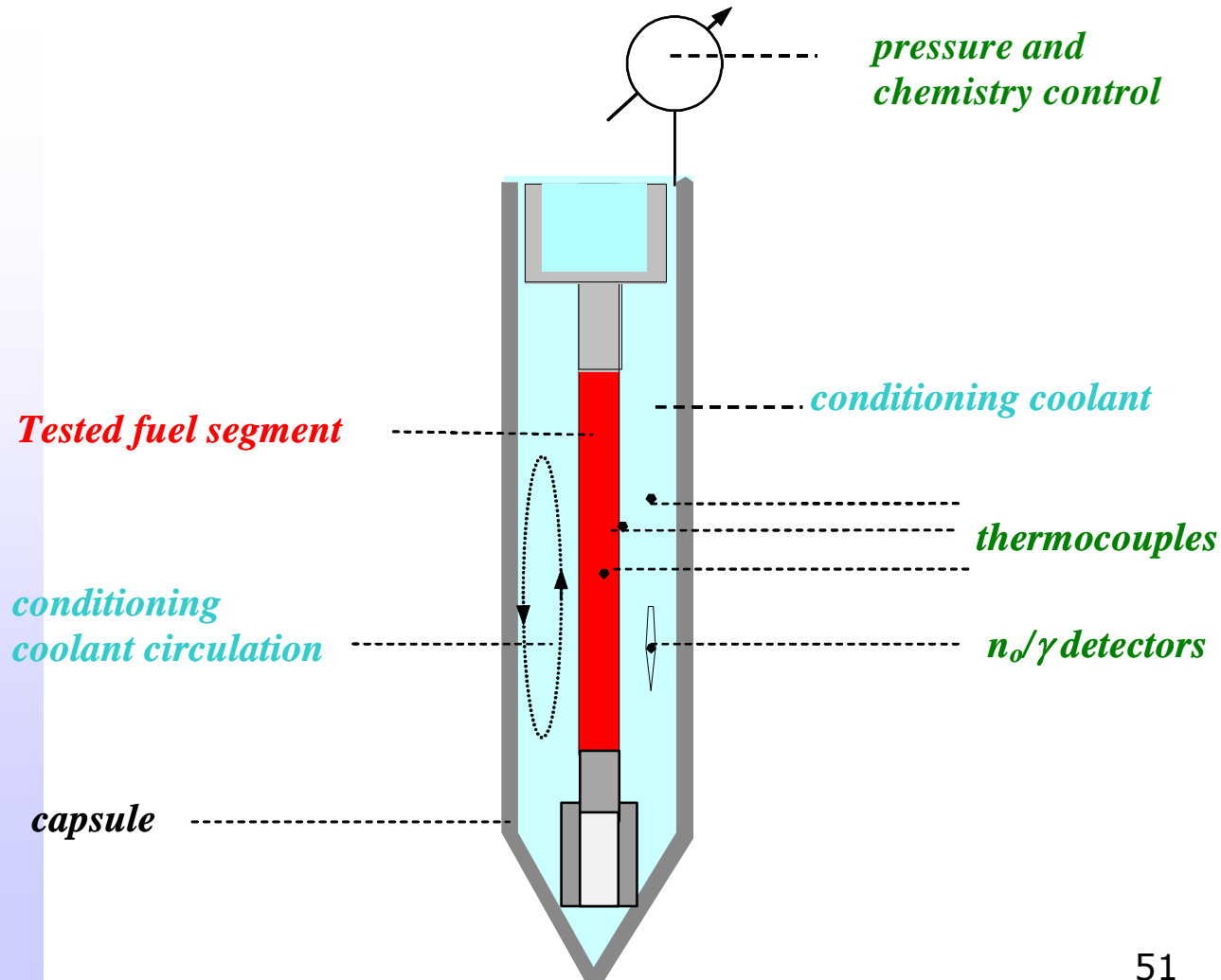
# 3. IPS Material Testing typical Layout



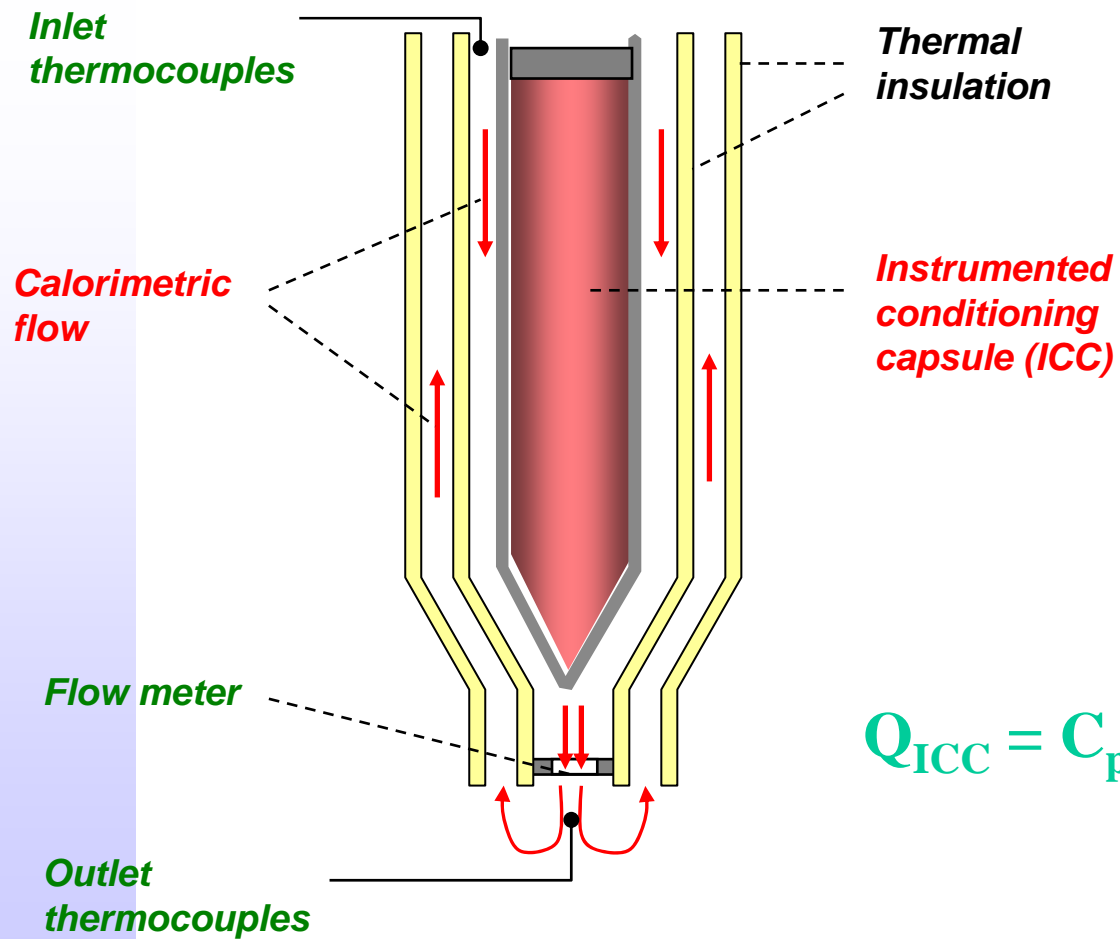
IPS outside diameter 80 mm  
 Relevant length for irradiation test 600 mm  
 Instrumentation : dosimeter, thermocouple, ..



### 3. Fuel Irradiation in MYRRHA Instrumented and Conditioned Capsule (ICC)

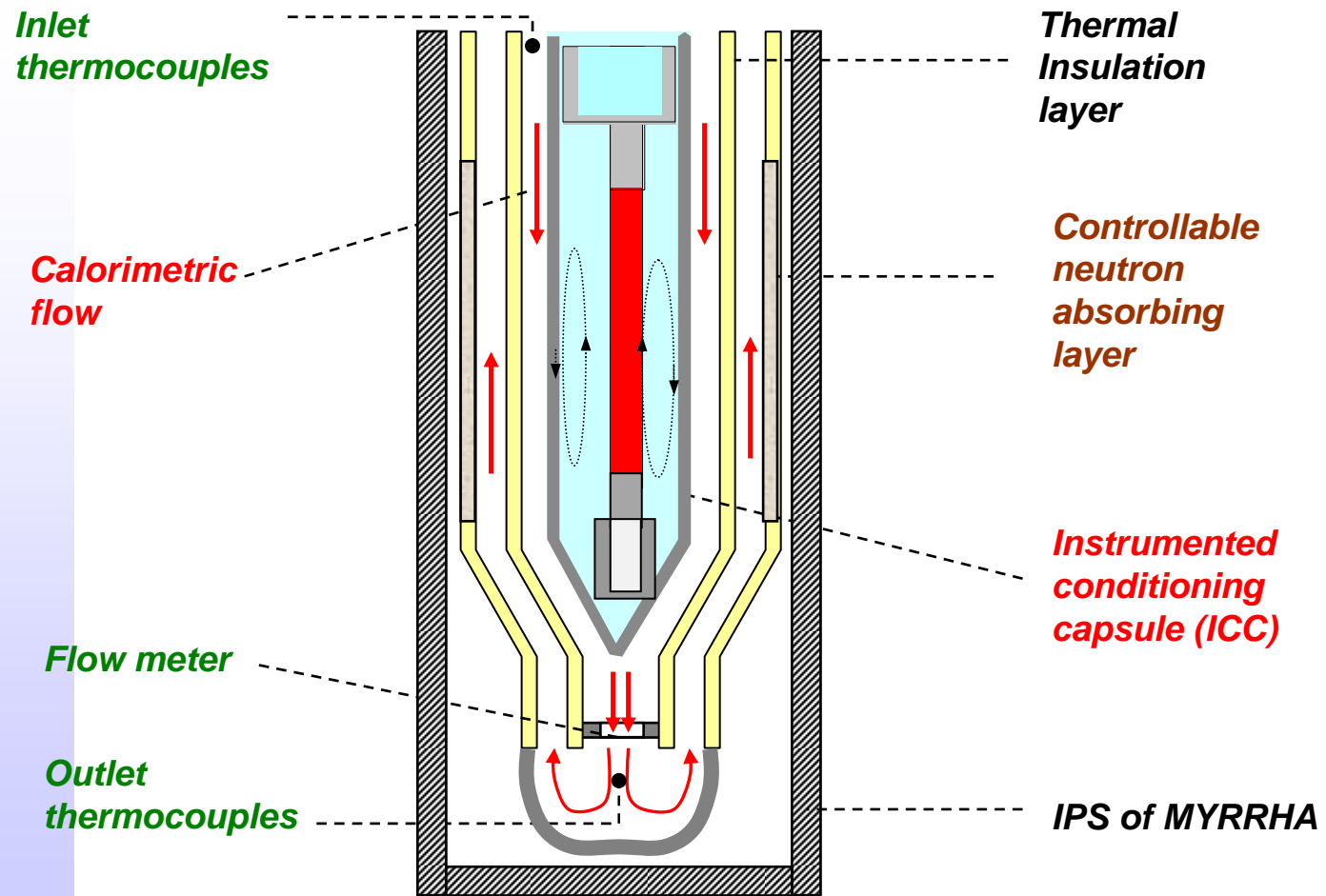


# 3. Fuel Irradiation in MYRRHA Calorimetric Calibration Device (CCD)

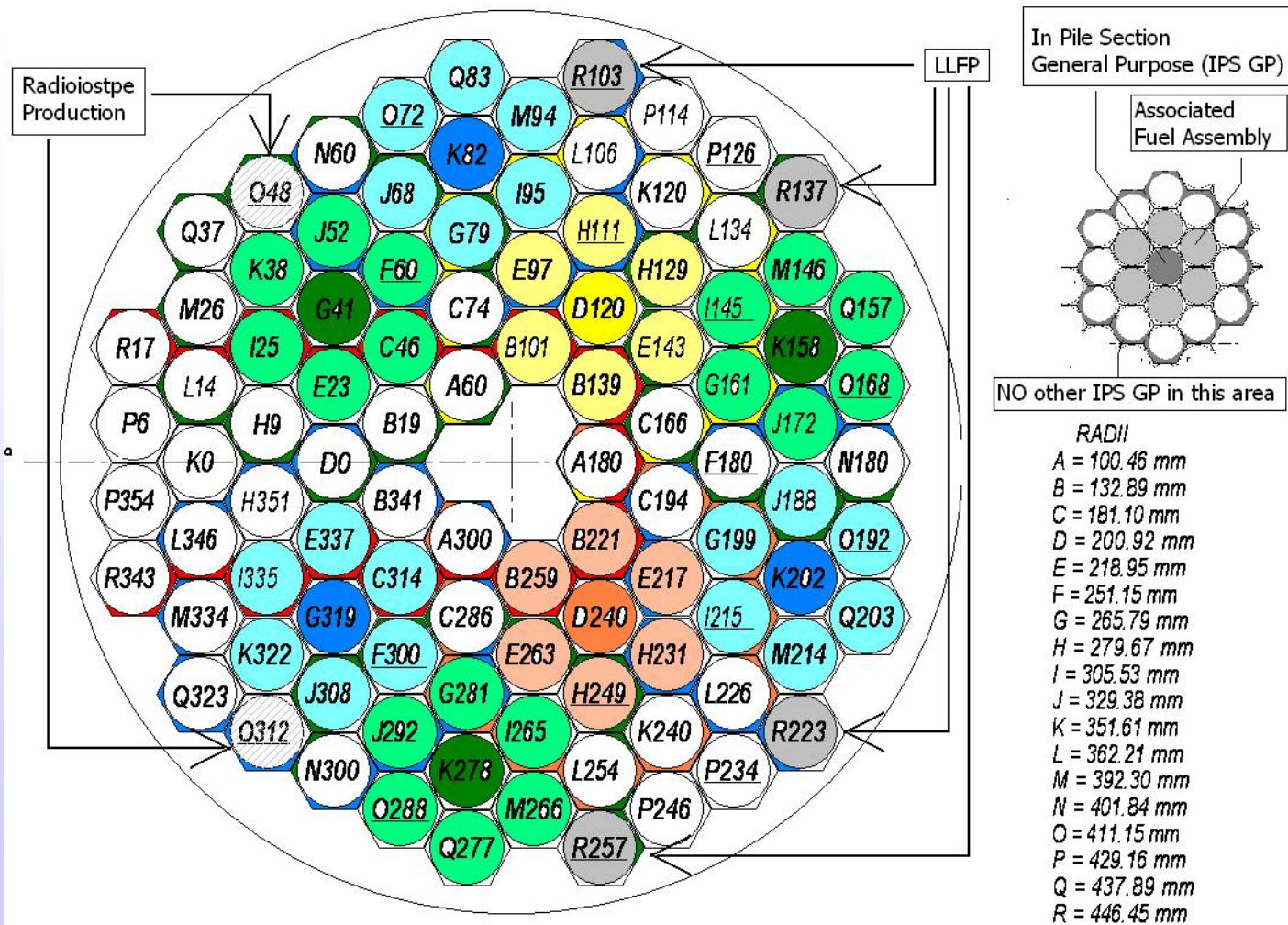


$$Q_{ICC} = C_{p \text{ cool}} \cdot G_{\text{cool}} \cdot \Delta T$$

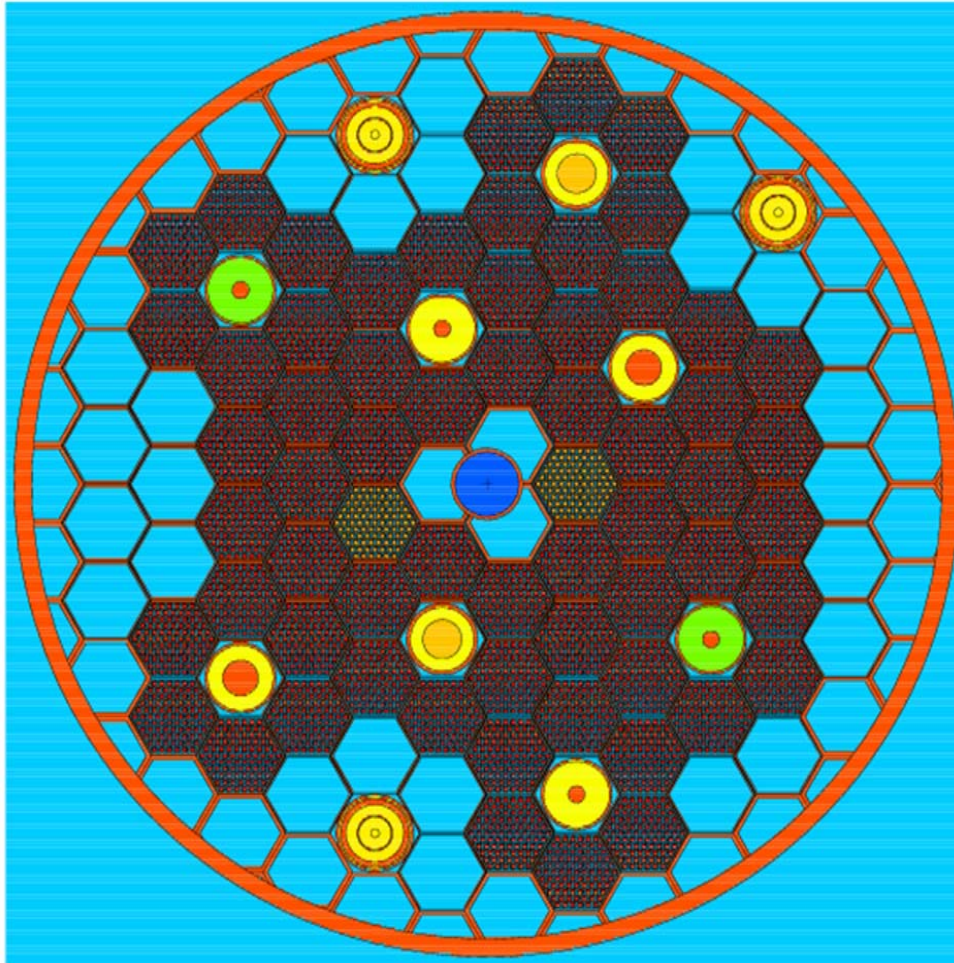
# 3. Fuel Irradiation in MYRRHA Instrumented and Conditioned Capsule in Calorimetric Calibration Device (ICC-CCD)



# 3. Accessible channels in MYRRHA Core for exp. rigs under reviewing for XT-ADS

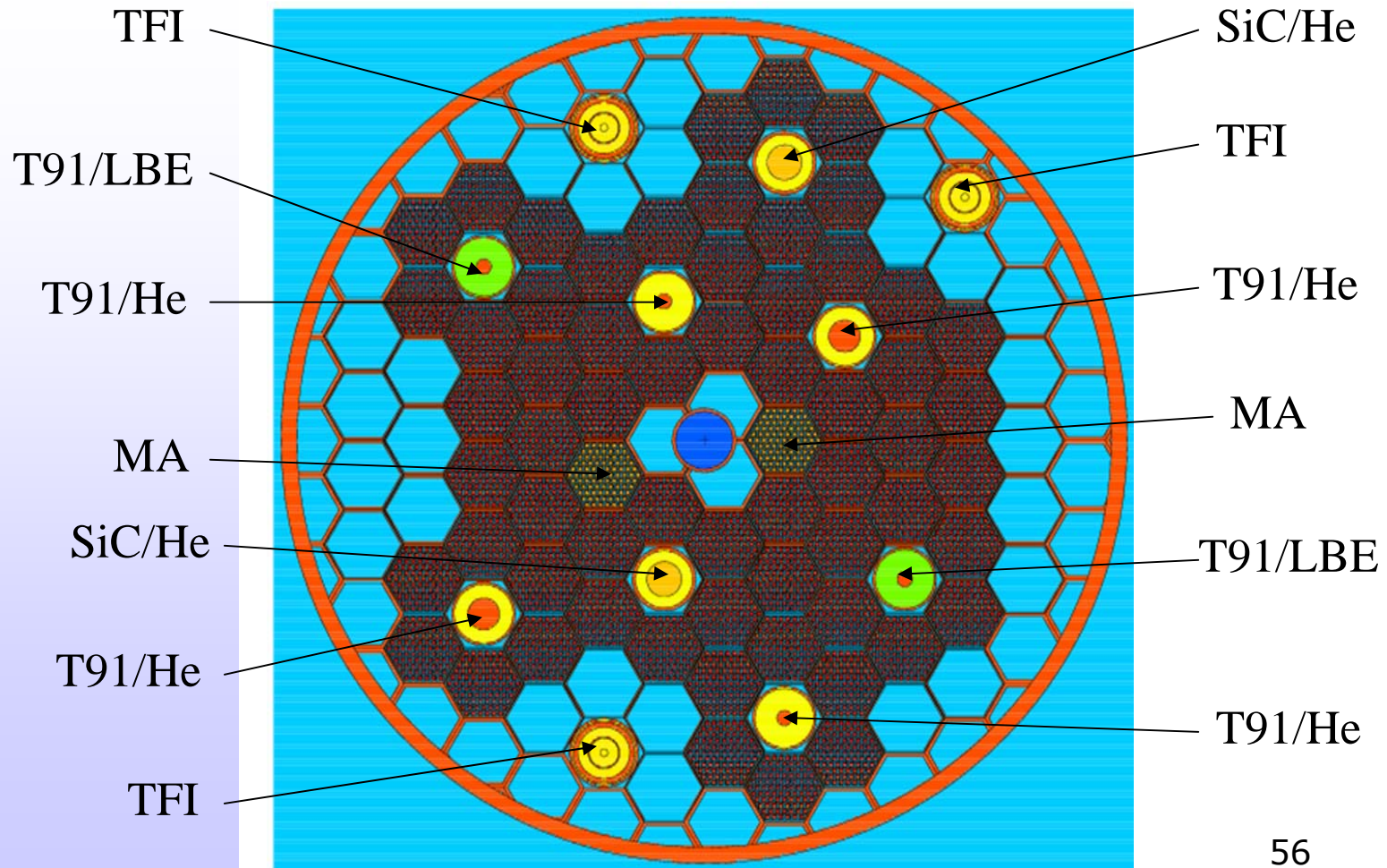


### 3. Typical MYRRHA core configuration with exp. rigs



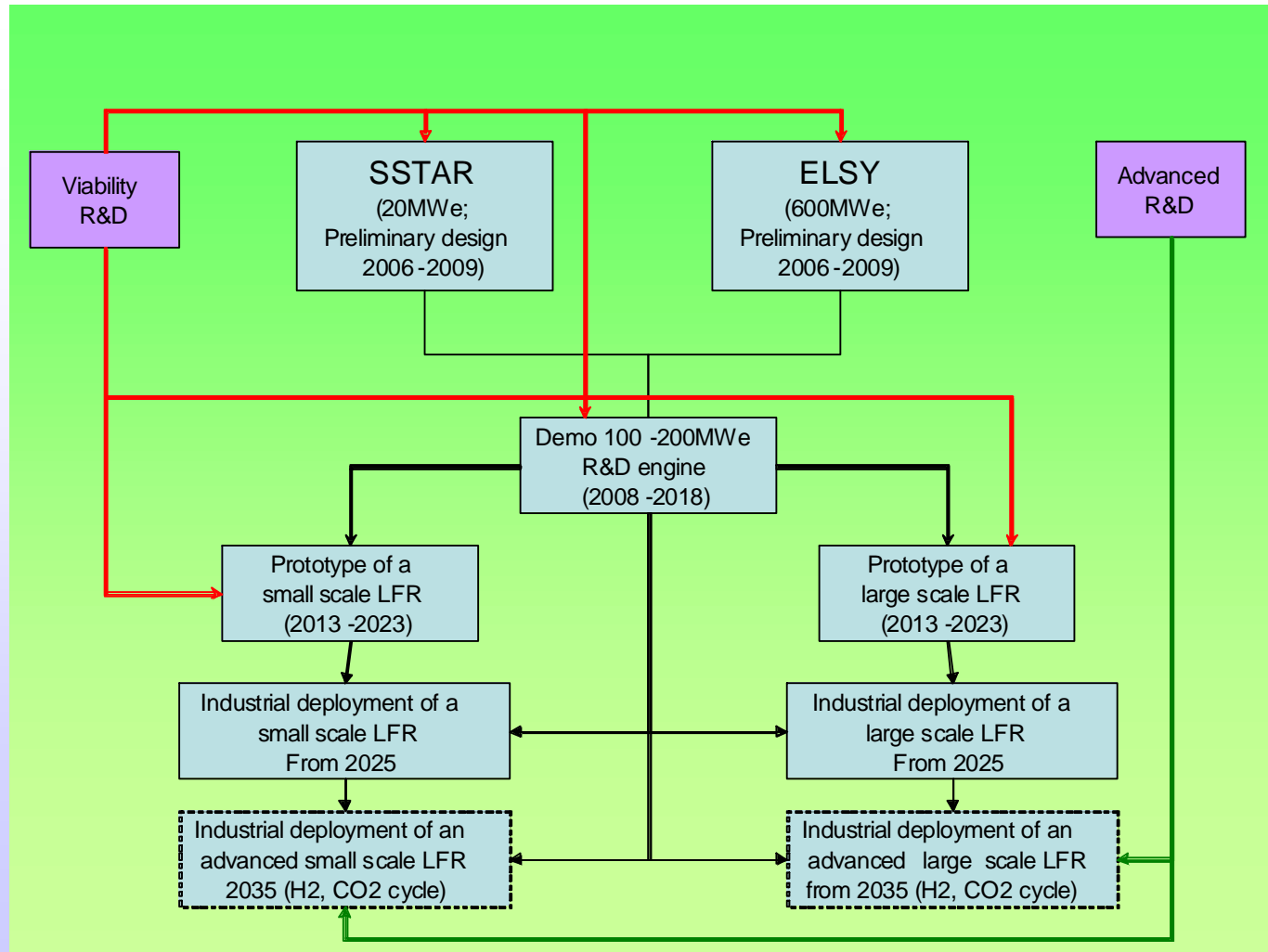
- 61 MOX-fuel assemblies
- 2 U-free MA (MgO matrix) assemblies
- 6 rigs with Steel samples
  - 2x2 He-cooled
  - 2 lead-cooled
- 2 rigs with SiC samples
- 3 H<sub>2</sub>O-moderated IPS
- $K_{eff} = 0.95181 \pm 0.00025$
- $K_s = 0.95960$
- Power : 52.3 MW

### 3. Fluxes and Cumulated DPA- damage (DPA/yr ; yr=365 EFPDs)





# 4. Link ADS – Gen. IV LFR



## 5-Well established and design driven support R&D Programme



- Pluri-annual R&D support programme established around the MYRRHA project inside SCK•CEN
- A bilateral collaboration network of quality
- The support R&D programme enhanced thanks to EUROTRANS

## 5. The MYRRHA R&D Programme



- Since the beginning of the MYRRHA project, we decided to accompany the project by a comprehensive support R&D programme including:
  - Windowless spallation target thermal-hydraulic design.
  - Vacuum Interface compatibility,
  - LBE technology: Po migration, visibility under LBE through ultrasonic cameras,
  - Material Corrosion & erosion and their mitigation,
  - LBE conditioning and monitoring,
  - Material embrittlement due to irradiation and LME,
  - MOX fuel qualification under LBE and irradiation up to high targeted burn up (100 GWd/t) and high dpa (100) and also under representative transient conditions,
  - Instrumentation development: O<sub>2</sub>-meters (< 200°C), HLM free surface monitoring, sub-criticality monitoring, ultrasonic visualisation
  - Robotics : development of a robot arm to be deployed under LBE for testing and qualification

## 5. MYRRHA Collaboration Network (1/3)



- **IBA**, Belgium: cyclotron design and/or Intermediate energy section of the LINAC (normal conducting);
- **ENEA**, Italy: spallation source thermal-hydraulics design, core dynamics;
- **UCL**, Belgium: spallation source design water experiment, CFD modelling, Advanced CFD development;
- **FZR**, Germany: instrumentation for the spallation target;
- **FZK**, Germany: windowless spallation source testing with Pb-Bi in KALLA, Material Corrosion studies, Neutronics of sub-critical systems;
- **NRG**, The Netherlands: Spallation Source CFD modelling and system safety assessment;

## 5. MYRRHA Collaboration Network (2/3)



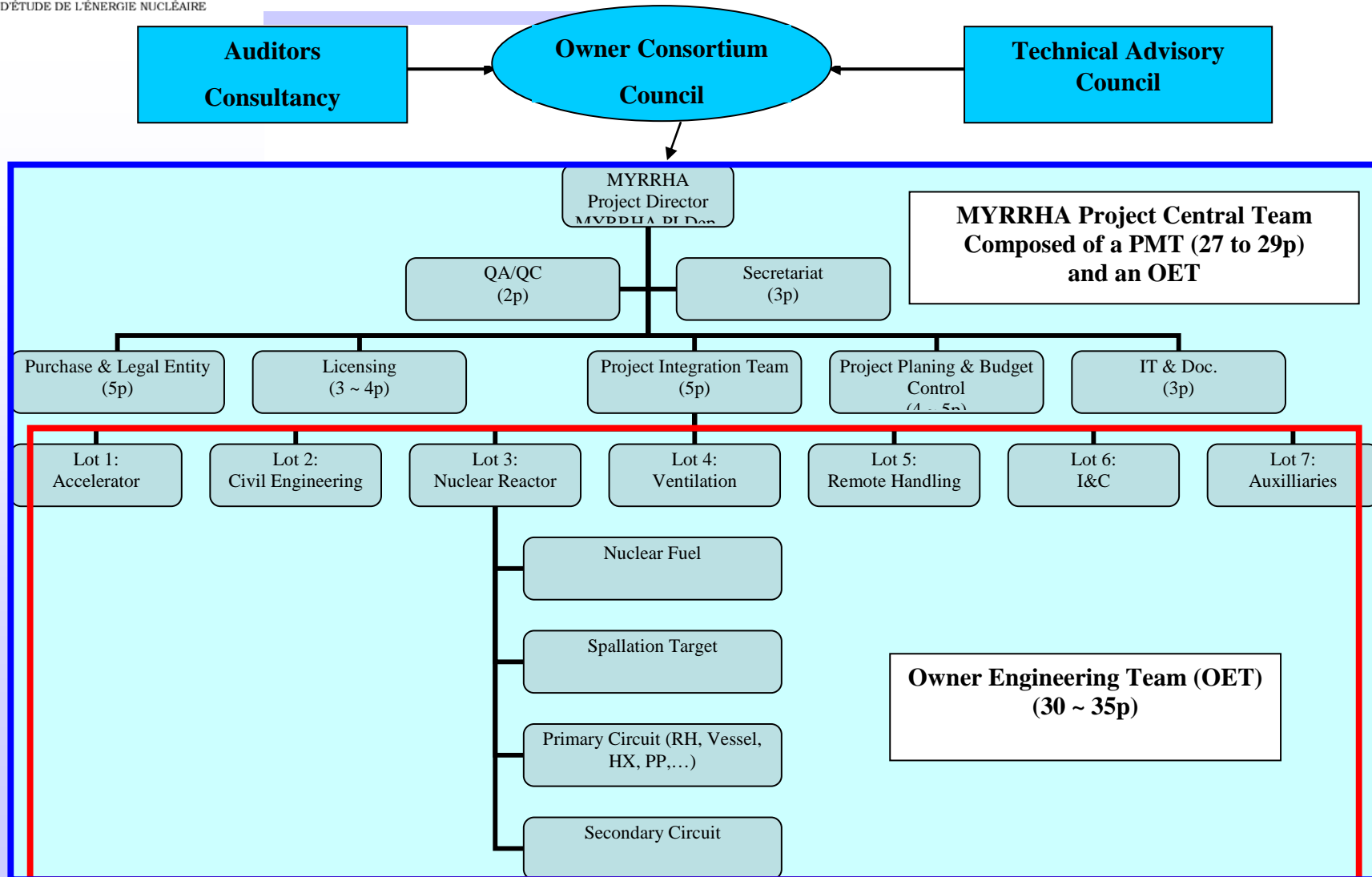
- **CEA**, France: subcritical core design, MUSE experiments;
- **CNRS/IN2P3**, France: LINAC development and components design, Windowless Spallation Target design, T91 structural material research, sub-critical core physics,
- **PSI**, Switzerland: basic spallation data, MEGAPIE;
- **IPUL**, Latvia: windowless spallation source testing with Hg,
- **Belgonucléaire**, Belgium: MOX Fuel manufacturer fuel pin and assembly design, fuel loading policy and fuel procurement;
- **CIEMAT**, Spain: Neutronic core design;
- **KTH**, Sweden: development and validation on basis of experimental results of adapted burn up codes for ADS,
- **IPPE**, Russia: design of the MYRRHA sub-critical reactor;

## 5. MYRRHA Collaboration Network (3/3)



- **Suez-Tractebel**, Belgium: confinement building and auxiliary systems, Safety analysis studies.
- **OTL**, UK: Remote Handling & Robotics design and development;
- **USI\_KU**, Lithuania: development of US sensors operational under LBE and aggressive radiation environment, development of associated visualisation camera and signal treatment;
- **AFCN and AVN**, Belgium: Licensing authorities
- **JAEA**, Japan : Material for fuel cladding, LBE technology, ADS Design
- **Contacts that may lead to additional collaborations exist with:**
  - **ISTC: JINR-Dubna, Russia, YALINA-Minsk, Belarus** (Through EUROTRANS)
  - **DoE and LANL; USA**
  - **CIAE, China**

# MYRRHA Project future organisation



## Roadmap of an XT-ADS at Mol (I)



- End 2008 → The conceptual design available.
- Informal discussions with the safety authorities → submit end of 2008 Preliminary Decommissioning Plan (PDP) to the waste management authorities – ONDRAF/NIRAS.
- 2009 – 2013 to work in parallel on:
  - 2009 – 2011 : detailed engineering design
  - 2012 – 2013: Drafting of the technical specifications of the different lots, the publication of the call for tenders, and awarding of the manufacturing contracts
  - 2009 – 2011 : In parallel testing of innovative components (for the accelerator and for the reactor);
  - 2009 – 2013 : Licensing and permitting → obtain the authorization of construction at the end of 2013



## Roadmap of an XT-ADS at Mol (II)

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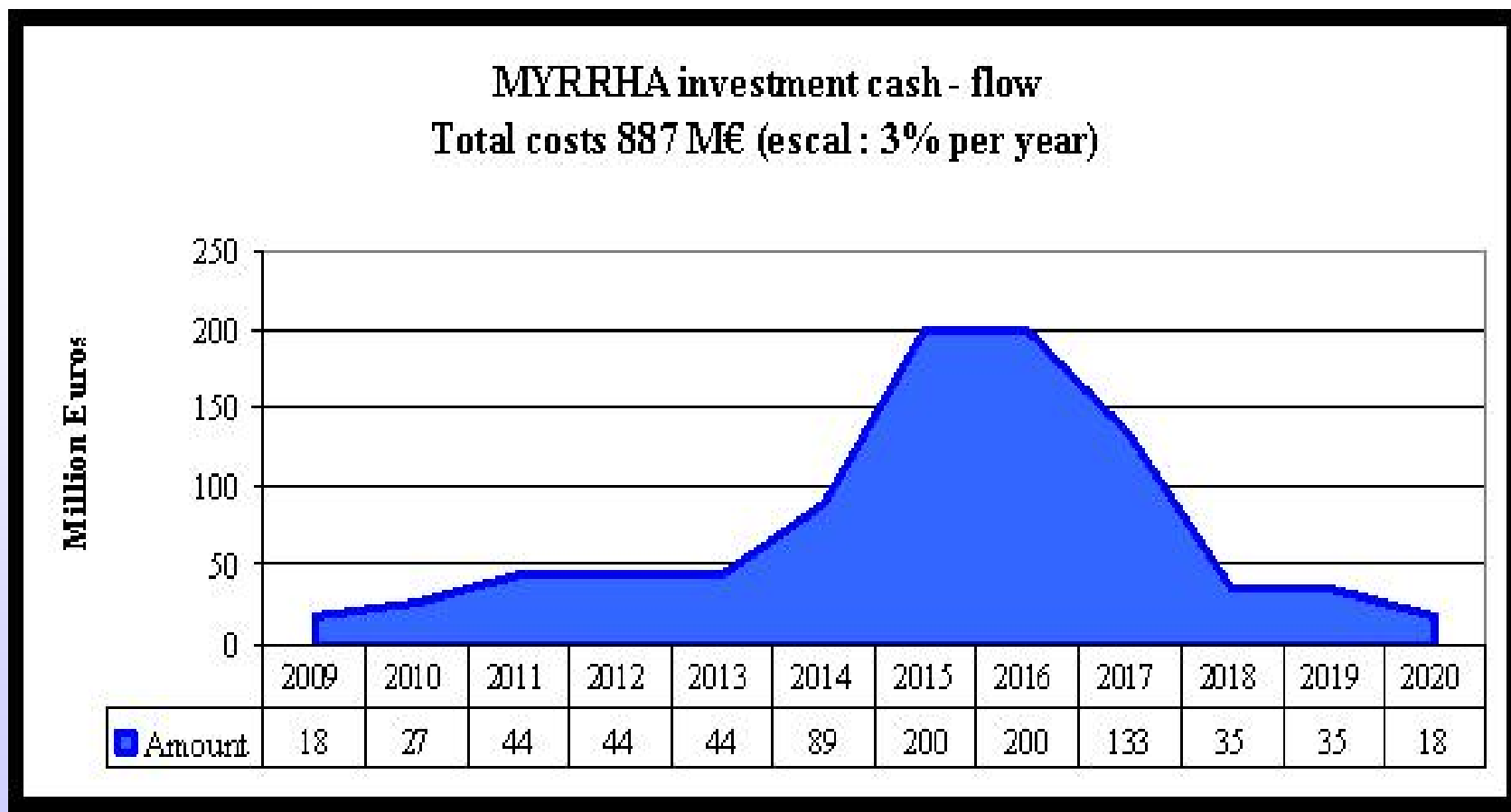
- 2014 – 2016 construction of components and the civil engineering works on the Mol site.
- 2017 Assembling together the different components
- 2018 – 2019 commissioning (at progressive levels of power).
- 2020 MYRRHA/XT-ADS full Power operation

# Summary of costs & contingencies:



- The total investment costs expressed in current value (2007) amounts to:
- 570 M€ without contingencies and 700 M€ with contingencies.
- In the 2007 MYRRHA project cost assessment, the project management costs are included.
- MYRRHA Project will be proposed as European open Research Facility for potential partners (Business plan 04.2007) will presented officially soon.
- First we are working for obtaining the Belgian support and commitment (Government, Industries, Universities)

# Financial Life Cycle



# One picture is better than a thousand words, we are in 2017~2020

